

Testing EULAG as a prospective dynamical core of the NWP model – results for a convective supercell

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Warsaw, Poland

INTRODUCTION

The objective of this experiment is to verify ability of the model to reconstruct a fully 3-dimensional problem related to the real atmosphere, with moist processes included (the next step after a series of 2D idealized dry tests).

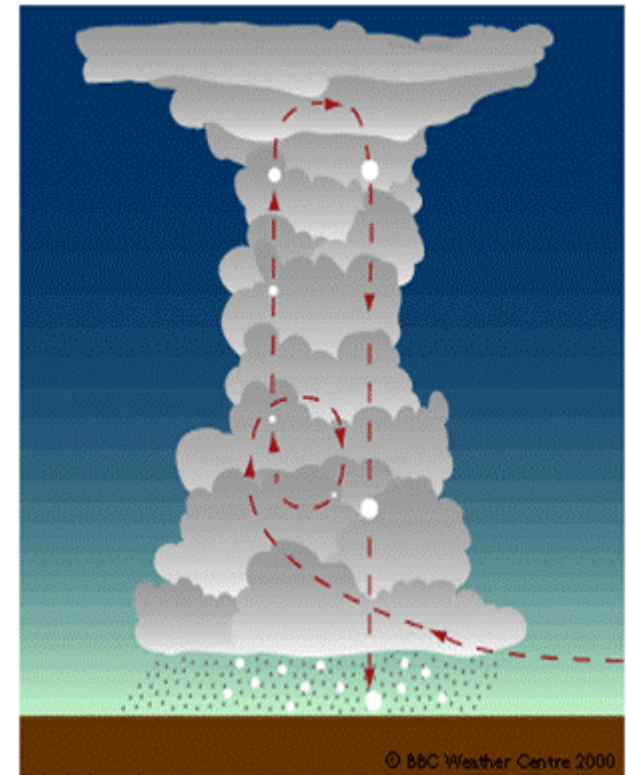
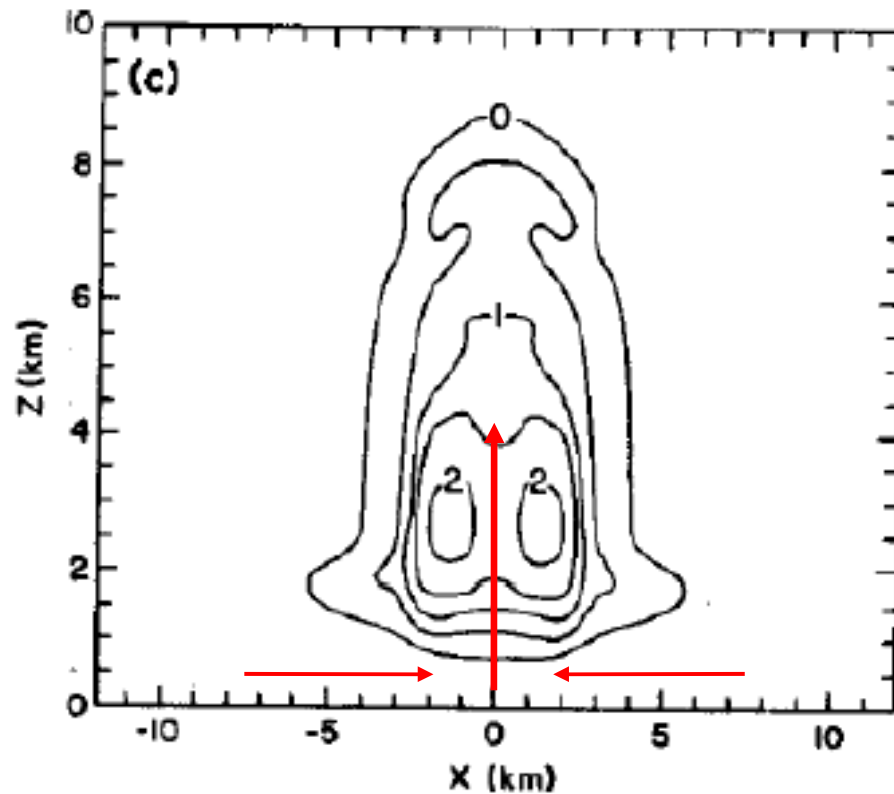
The two reference experiments:

1. Klemp and Wilhelmson, 1978, JAS (KW78)
2. Weisman and Klemp, 1982, MWR (WK82)

Both were simulated using anelastic nonhydrostatic model EULAG.

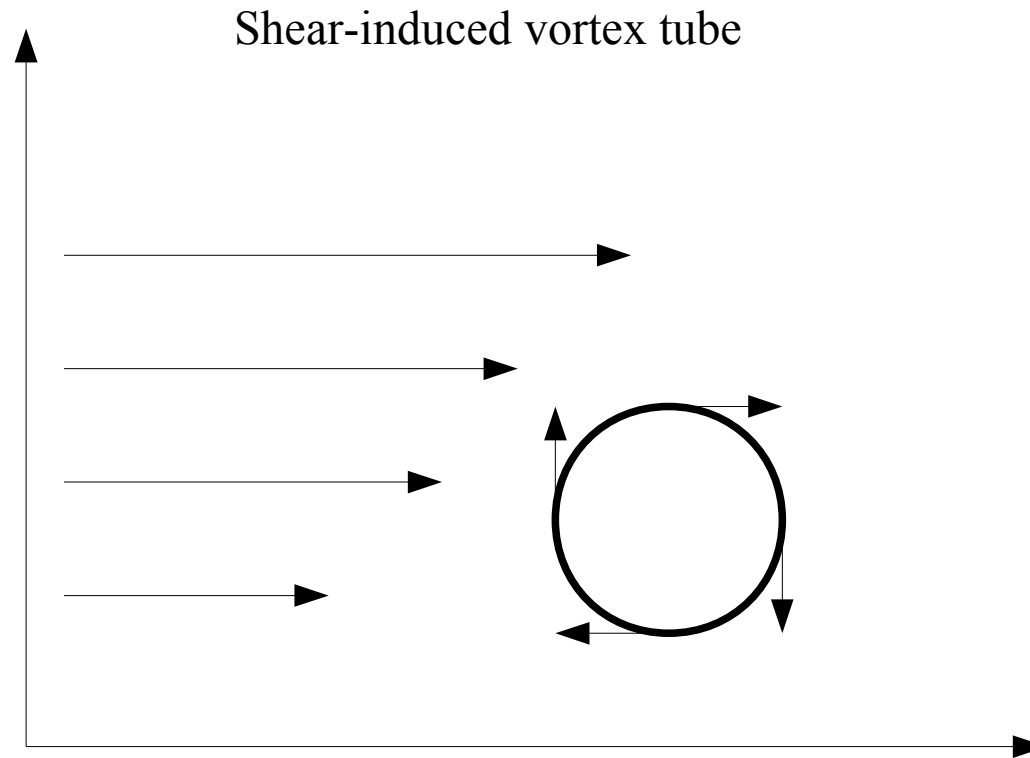


SUPERCELL – HOW IT WORKS?



$$CAPE = \int_{z_f}^{z_n} g \left(\frac{T_{v_{parcel}} - T_{v_{env}}}{T_{v_{env}}} \right) dz$$

SUPERCELL – HOW IT WORKS?



SUPERCCELL – HOW IT WORKS?

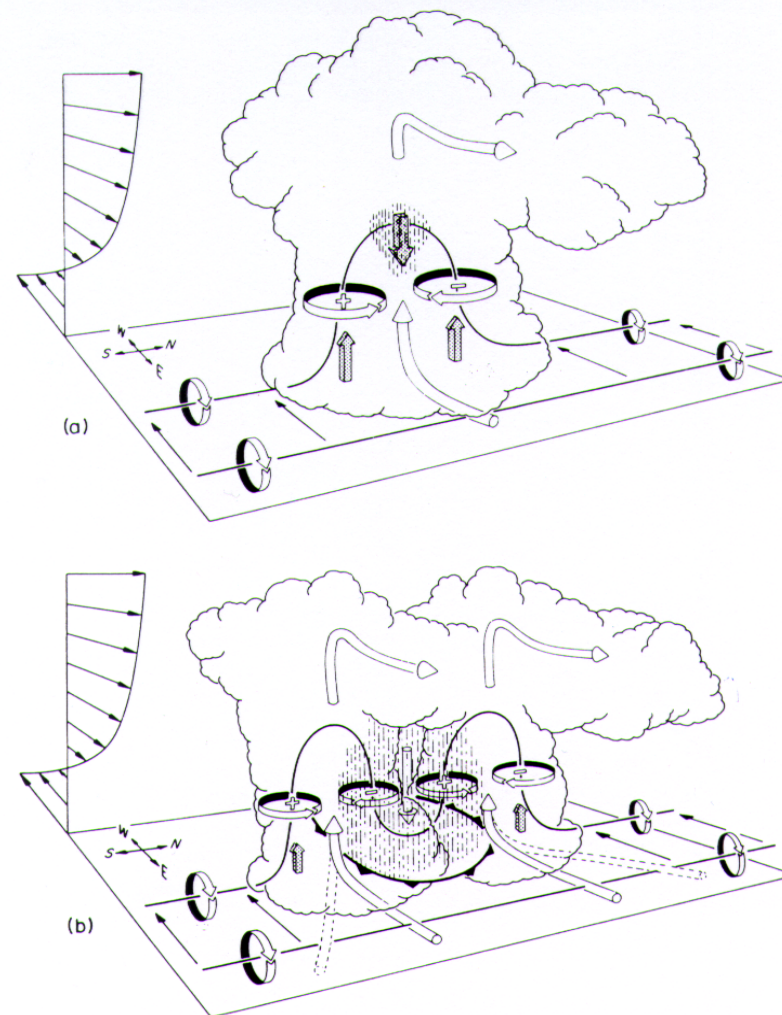
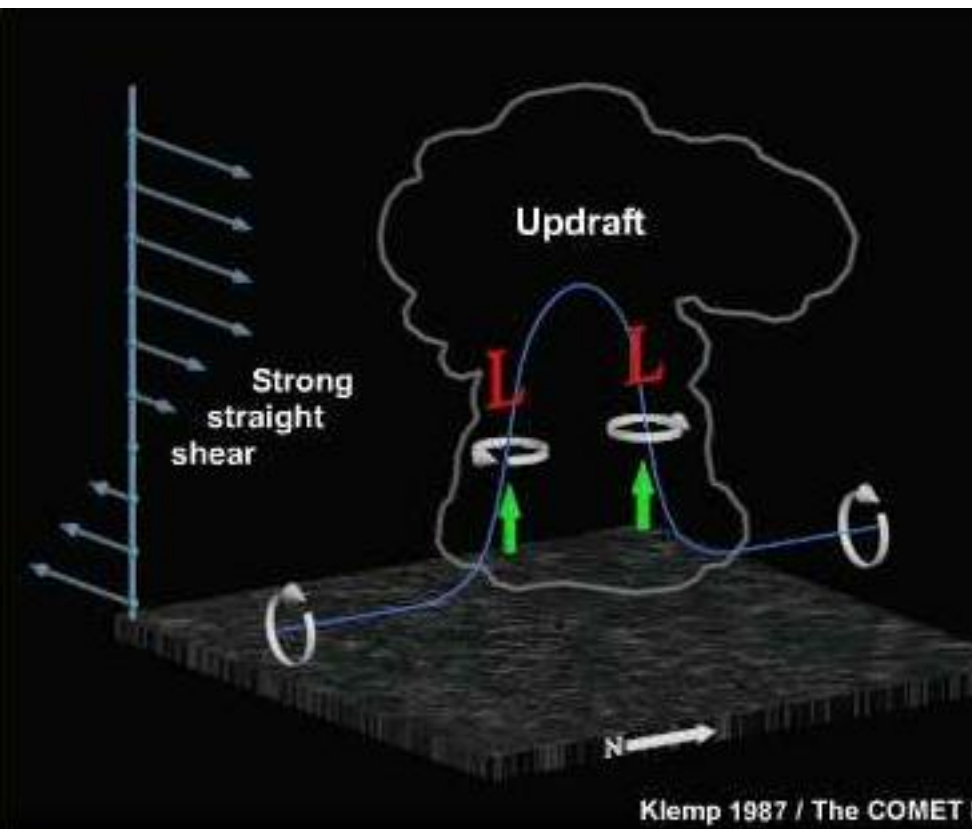
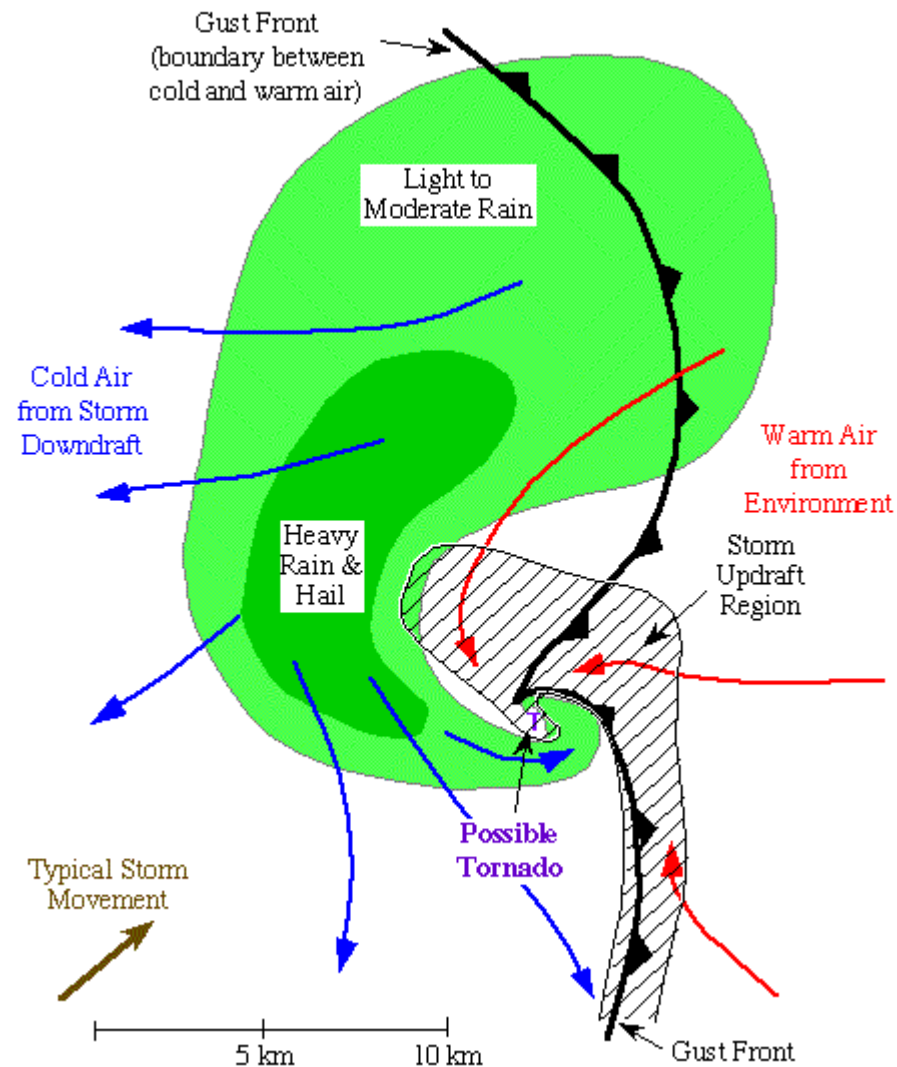


Fig. 11.28 Schematic drawing showing the deformation of vortex tubes (solid lines) by evolving supercell convection in unidirectional shear. Cylindrical arrows show the direction of storm-relative flow. Shaded arrows depict accelerations due to nonhydrostatic pressure perturbations and water loading and evaporation. [From Klemp (1987).]

SUPERCCELL – HOW IT WORKS?

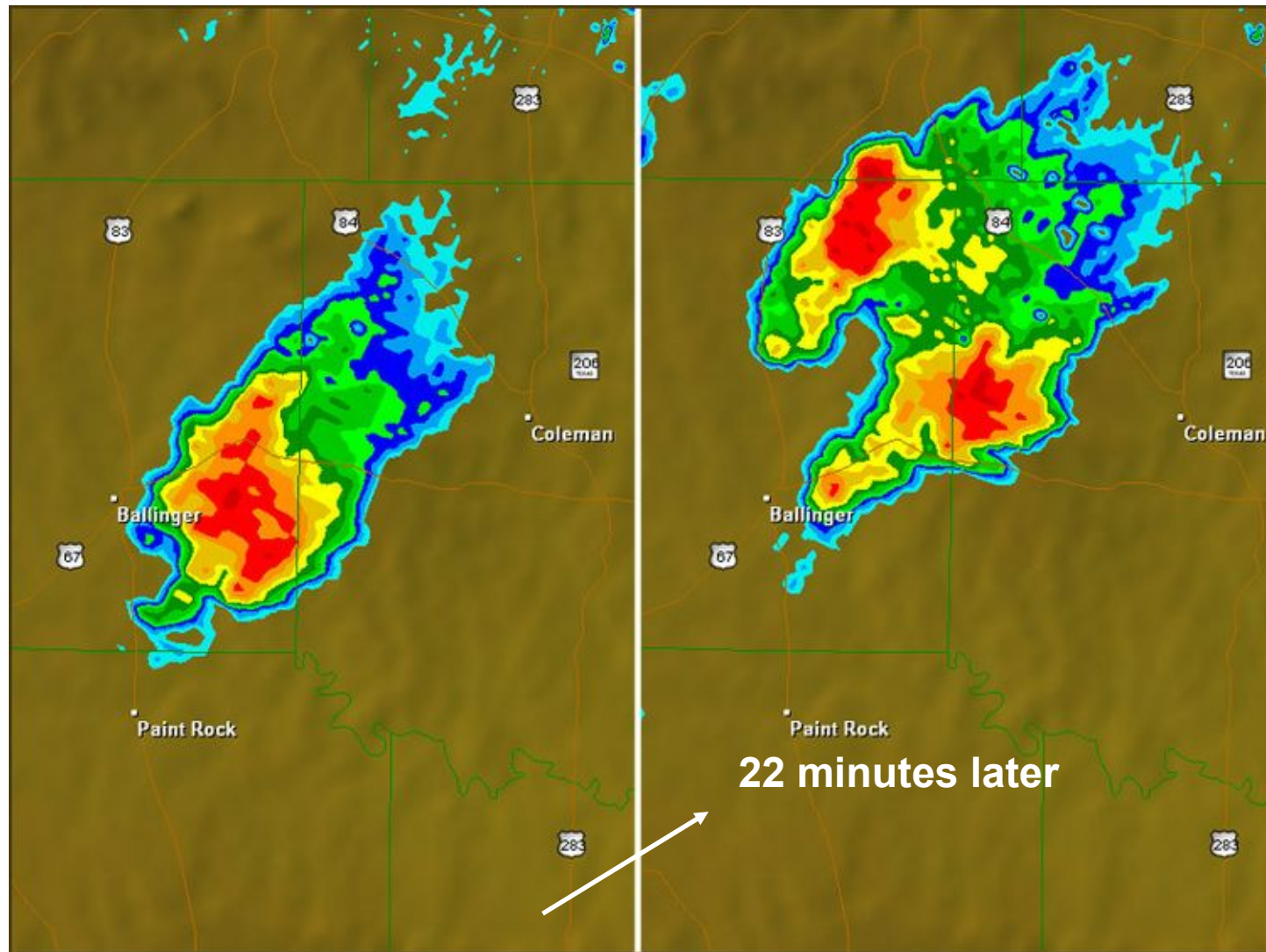
Schematic of Surface Conditions Common with a Supercell Thunderstorm



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SUPERCCELL – HOW IT WORKS?



NOAA Doppler radar reflectivity (Texas, 2008)

The Simulation of Three-Dimensional Convective Storm Dynamics

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(Manuscript received 22 September 1977, in final form 21 February 1978)



Grid: uniform,

dx=dy=1km, dz=500m

domain size: 24x24x10 km (additionally 32x32 and 256x256)

Subgrid-scale processes:

1) TKE scheme, Pr=0.33 $K_m = c_m T K E^{1/2} (\Delta x \Delta y \Delta z)^{1/3}$

2) ILES (implicit large-eddy simulation)

Moist processes:

bulk parametrization (instantaneous saturation adjustment,

Kessler scheme, warm rain only)

$$A_r = k_1 (q_c - a),$$

Boundary conditions:

open b.c. (additionally periodic)

$$C_r = k_2 q_c q_r^{0.875},$$

Initial conditions:

realistic sounding

$$E_r = \frac{1}{\bar{p}} \frac{(1 - q_v/q_{vs}) C (\bar{p} q_r)^{0.525}}{5.4 \times 10^5 + 2.55 \times 10^6 / (\bar{p} q_{vs})},$$

Time integration:

24 min for unsheared environment

36 min for a shear flow

40 min for veering wind

$$V = 3634 (\bar{p} q_r)^{0.1346} \left(\frac{\bar{p}}{\rho_0} \right)^{-\frac{1}{2}},$$

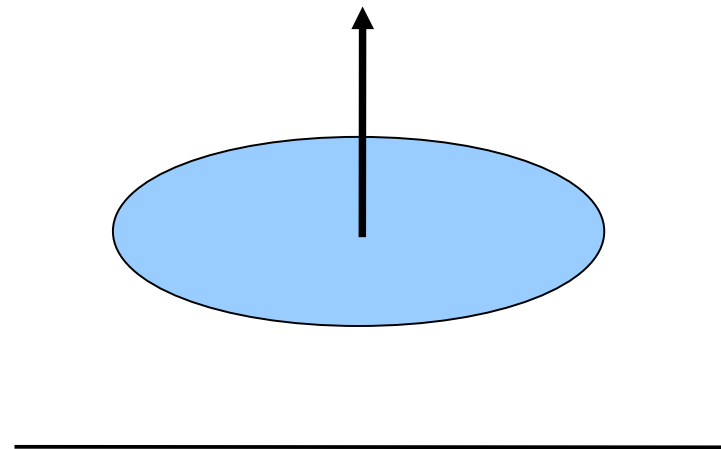
Details of setup agreed (?) with KW78



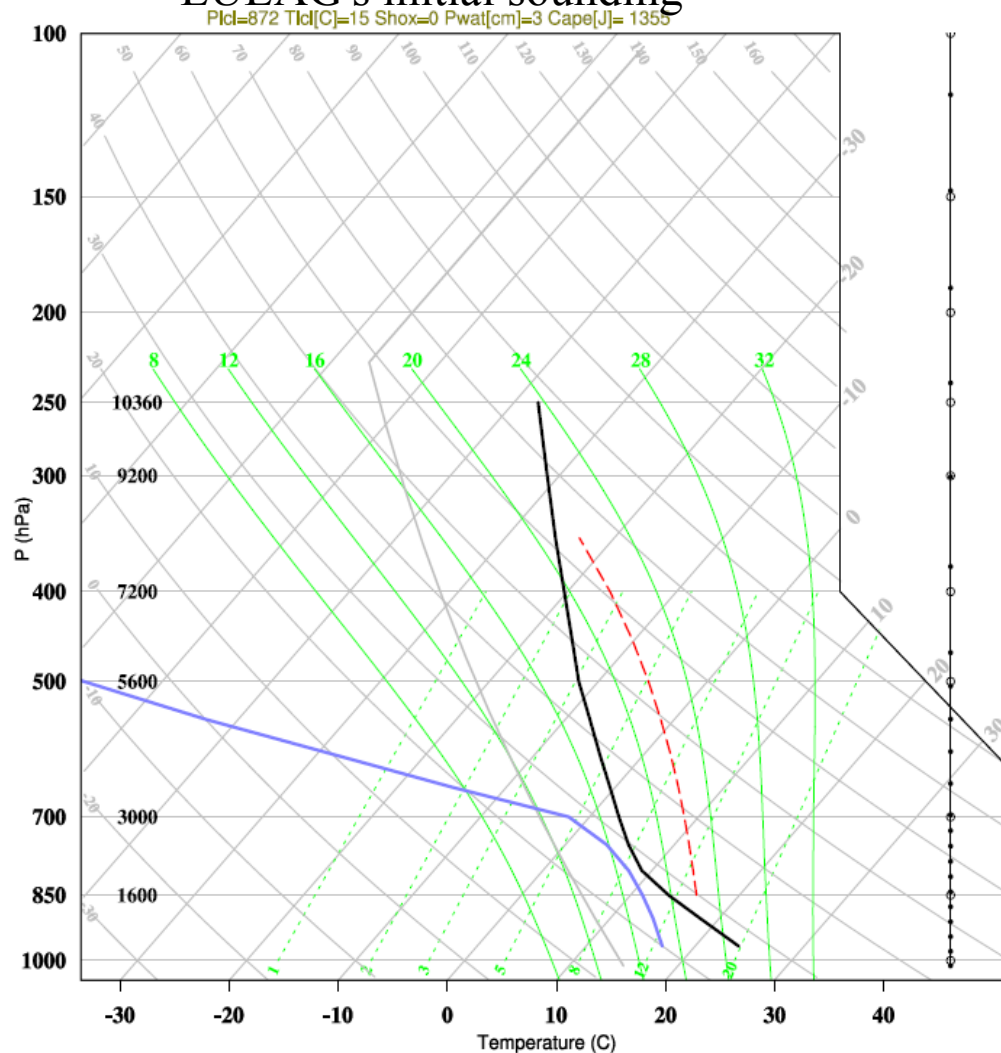
$$\theta' = \Delta\theta_0 \cos^2 \frac{1}{2} \pi \beta$$

$$\beta = \left(\left(\frac{x - x_c}{x_r} \right)^2 + \left(\frac{y - y_c}{y_r} \right)^2 + \left(\frac{z - z_c}{z_r} \right)^2 \right)^{1/2}$$

$$z_c = 1500 \text{ m}, x_r = y_r = 10.8 \text{ km}, z_r = 2000 \text{ km and } \Delta\theta = 1.5^\circ \text{ C}$$

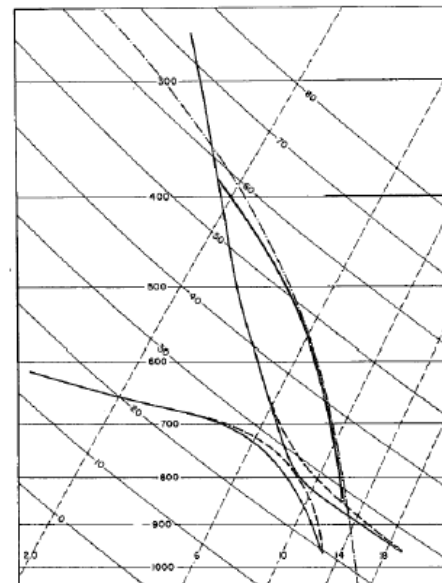


EULAG's initial sounding



EULAG's initial profiles of temperature and humidity - from Fig.1 of KW78. Accuracy of the profile is limited. Slight ($\sim 0.2\text{K}$) modifications of the temperature at different levels may significantly change CAPE ($\sim 5\text{-}10\%$)

KW78

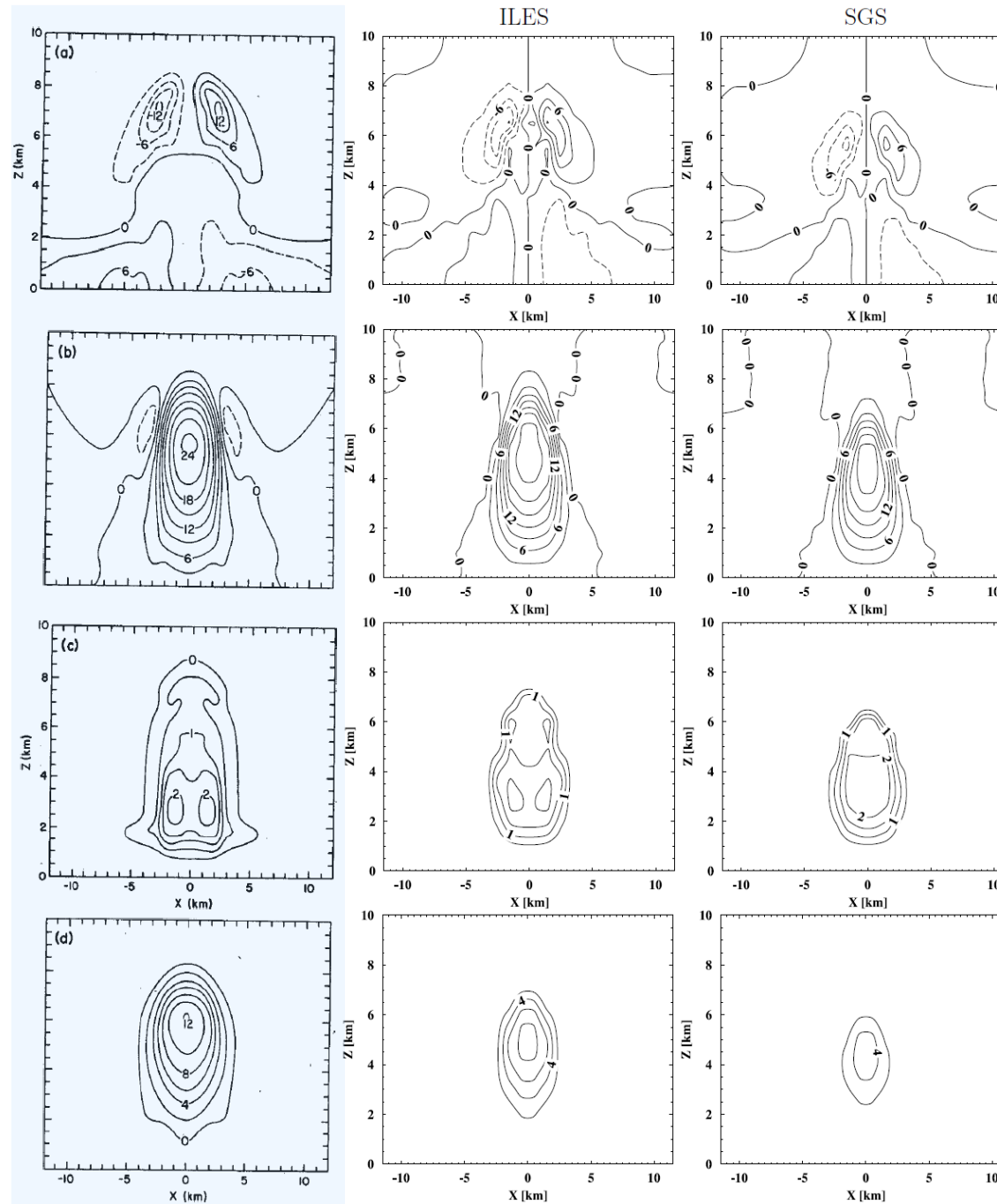


U (m/s)
 $\Delta U = 3 \text{ m/s}$

W (m/s)
 $\Delta W = 3 \text{ m/s}$

qc (g/kg)
 $\Delta qc = 0.5 \text{ g/kg}$

qr (g/kg)
 $\Delta qr = 2 \text{ g/kg}$



X-Z crossection at
 $y=0$

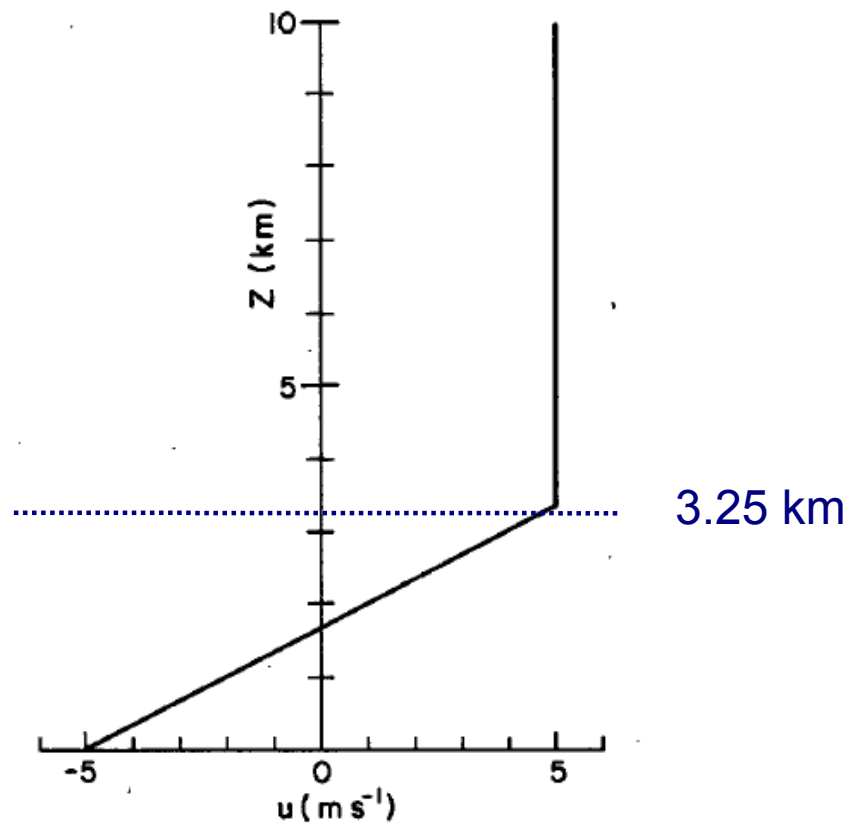
time=24min

ILES – implicit
large-eddy
simulation (no
explicit subgrid-
scale mixing)

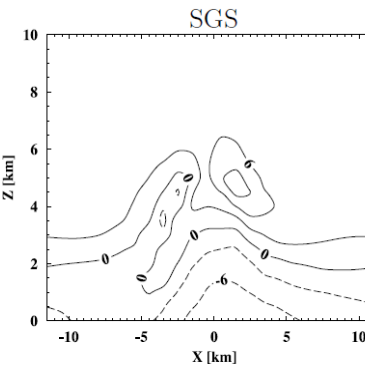
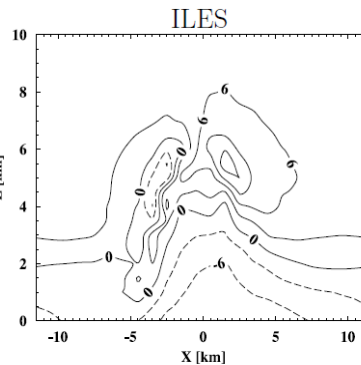
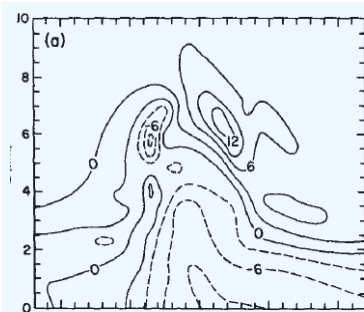
SGS – explicit
subgrid-scale
mixing
parametrization
used



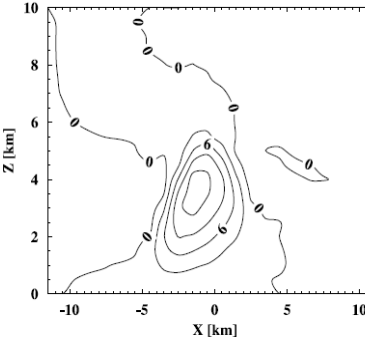
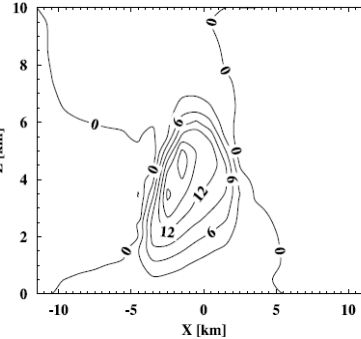
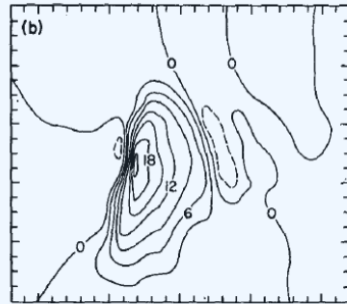
Idealized external shear flow:



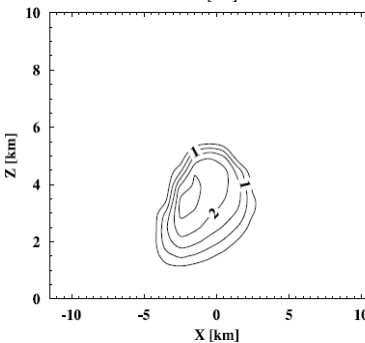
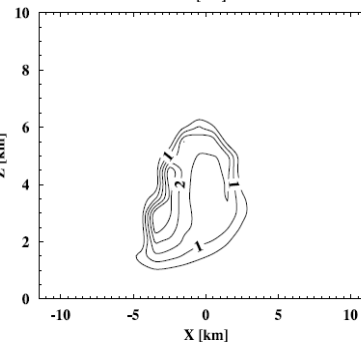
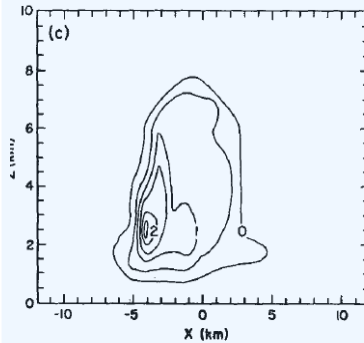
U (m/s)
 $\Delta U = 3 \text{ m/s}$



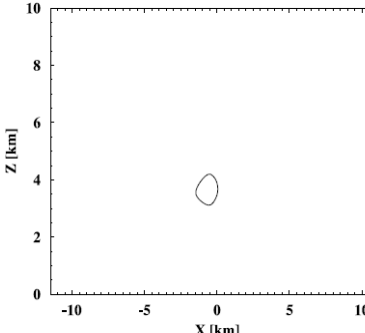
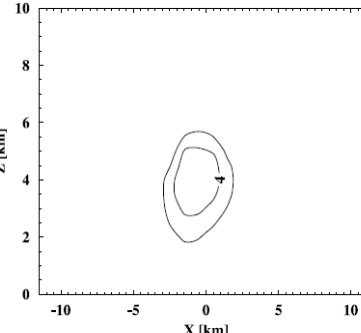
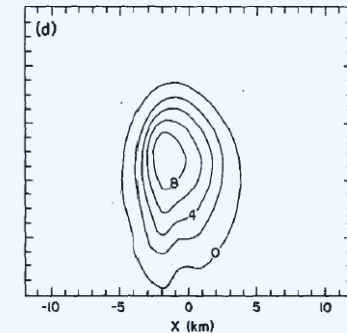
W (m/s)
 $\Delta W = 3 \text{ m/s}$



qc (g/kg)
 $\Delta qc = 0.5 \text{ g/kg}$

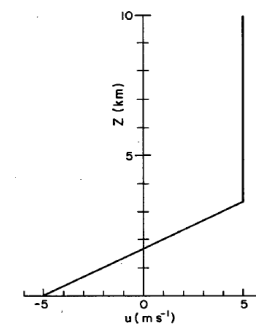


qr (g/kg)
 $\Delta qr = 2 \text{ g/kg}$



X-Z crossection at
 $y=0$

time=24min

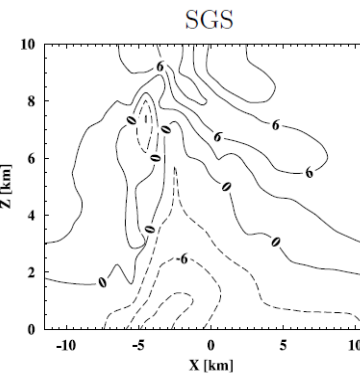
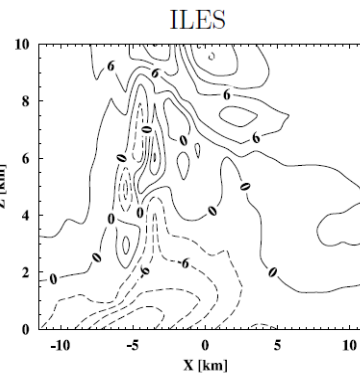
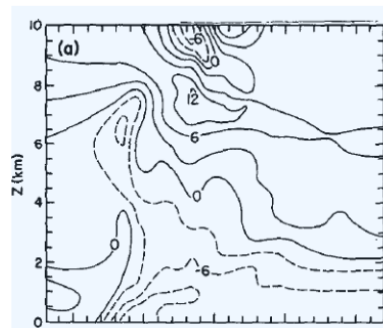


ILES – implicit
large-eddy
simulation (no
explicit subgrid-
scale mixing)

SGS – explicit
subgrid-scale
mixing
parametrization



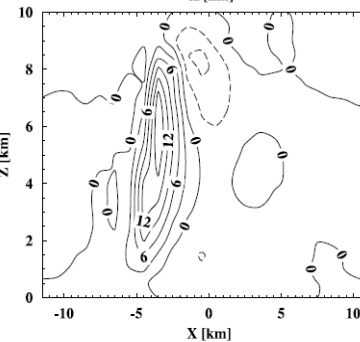
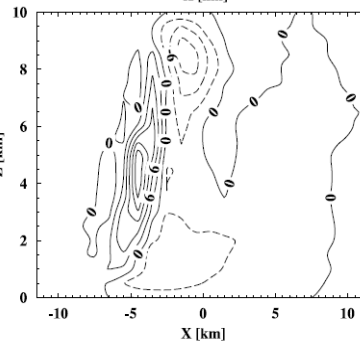
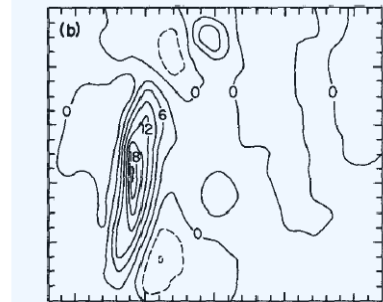
U (m/s)
 $\Delta U = 3 \text{ m/s}$



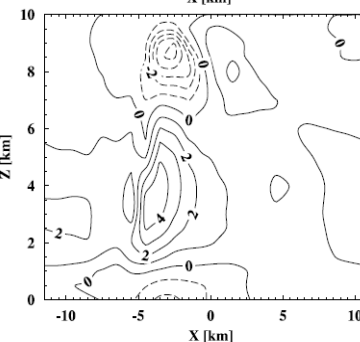
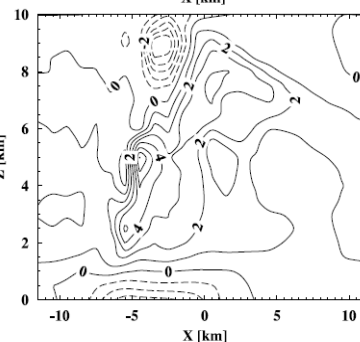
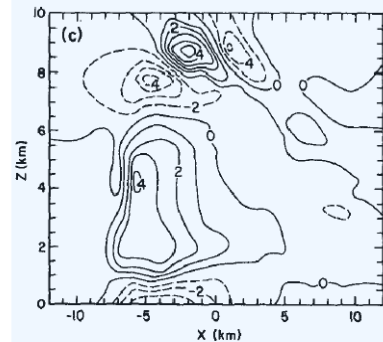
X-Z crossection at
 $y=0$

time=36min

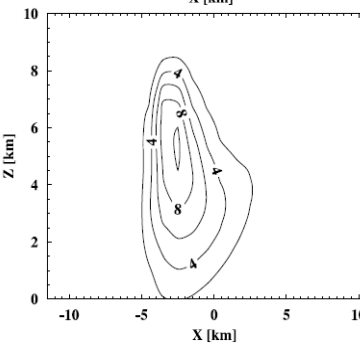
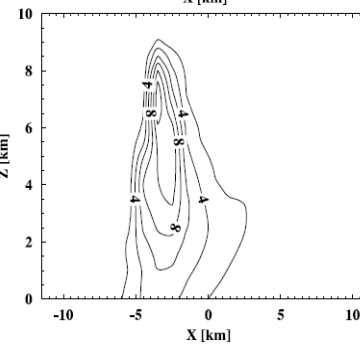
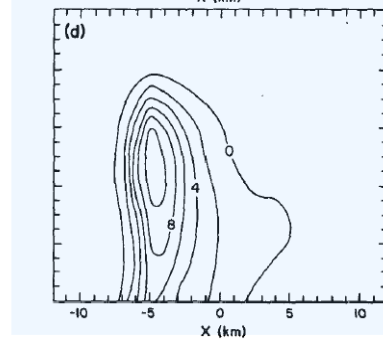
W (m/s)
 $\Delta W = 3 \text{ m/s}$



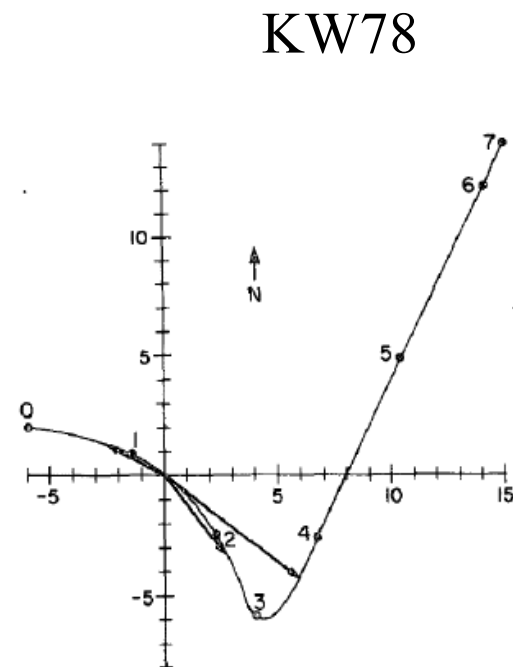
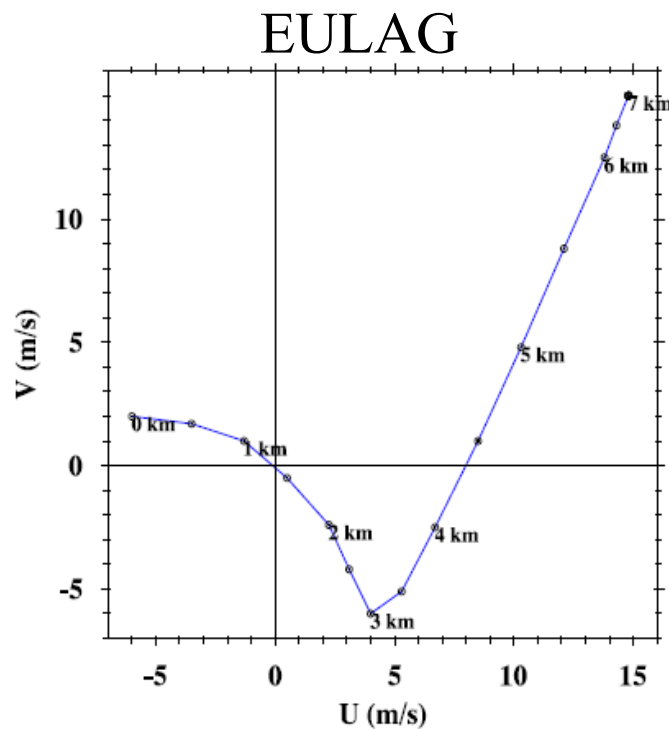
Θ (K)
 $\Delta \theta = 1 \text{ K}$



qr (g/kg)
 $\Delta qr = 2 \text{ g/kg}$

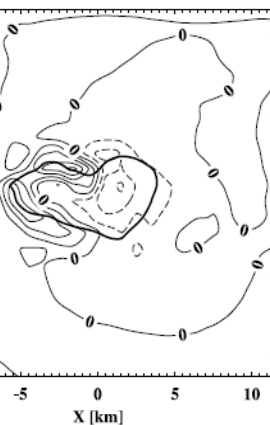
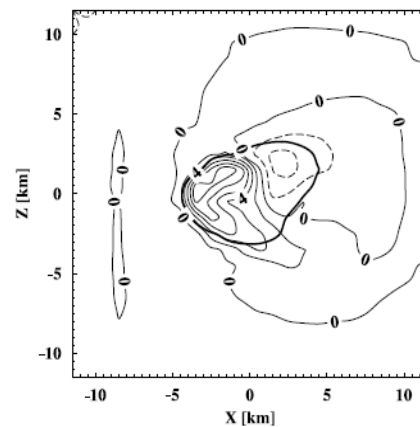
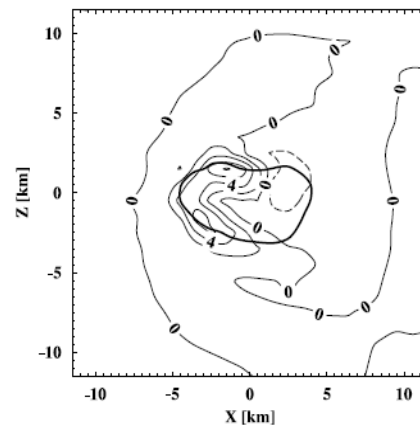
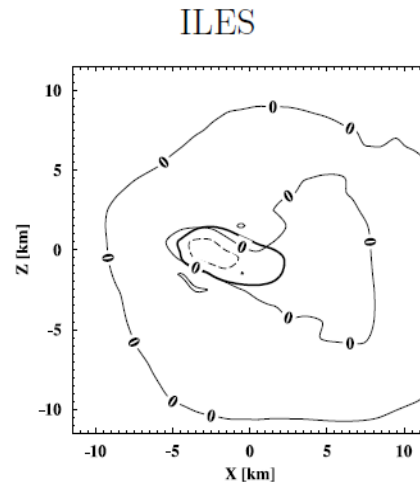
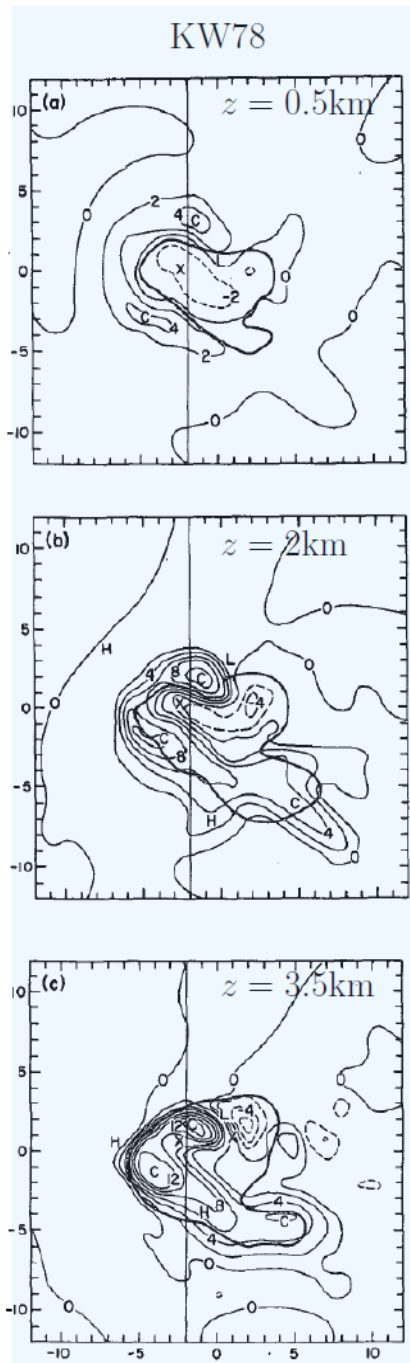


Hodograph of horizontal velocity



Comparison of vertical velocity field

- $w > 0$ m/s
- $w < 0$ m/s
- $qr > 1$ g/kg



X-Y crossection at
 $y = 0.5$ km, $y = 2$ km
 and $y = 3.5$ km

time = 40 min

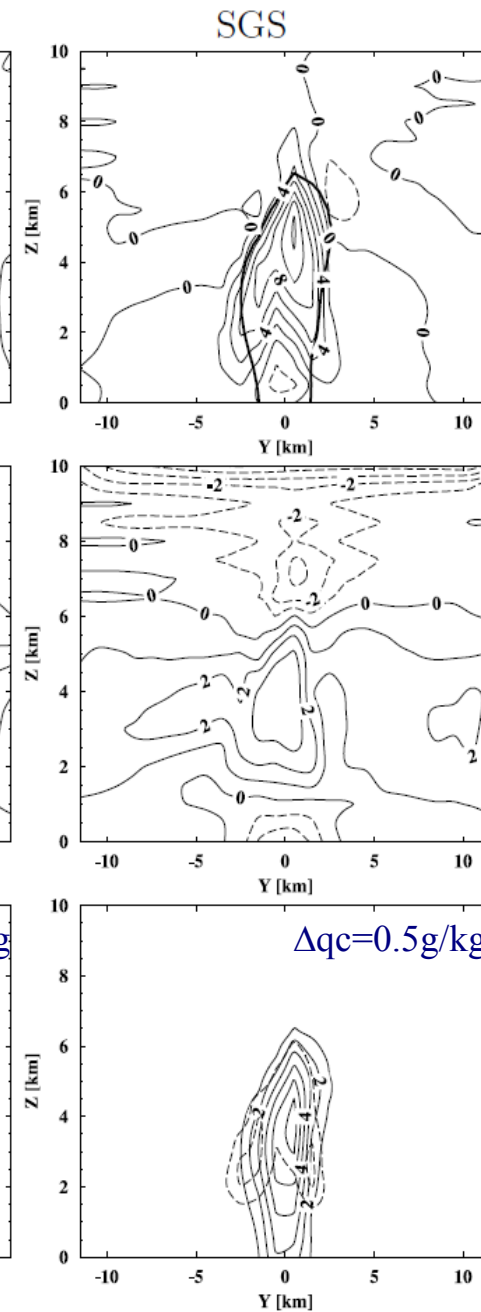
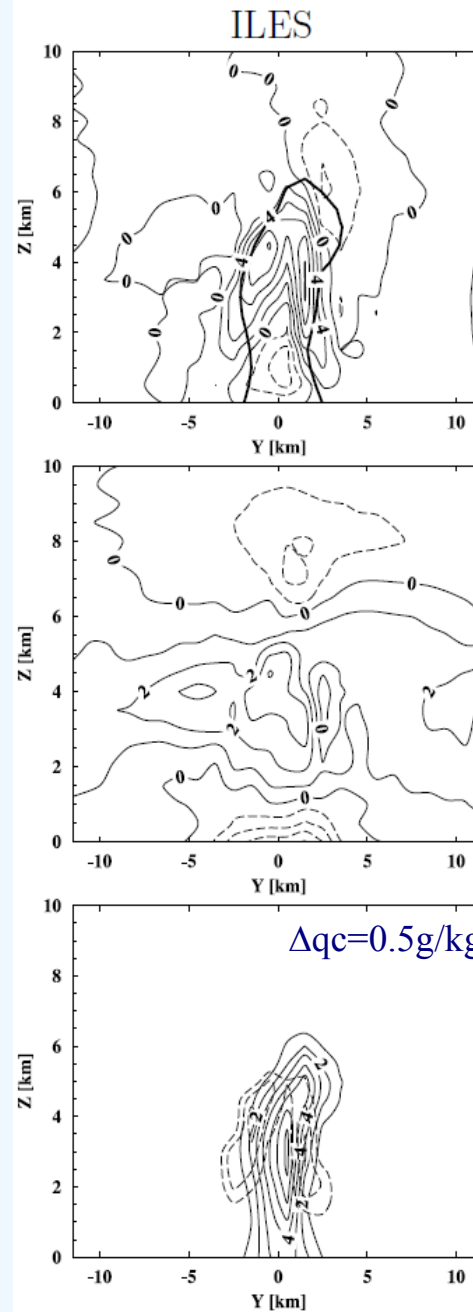
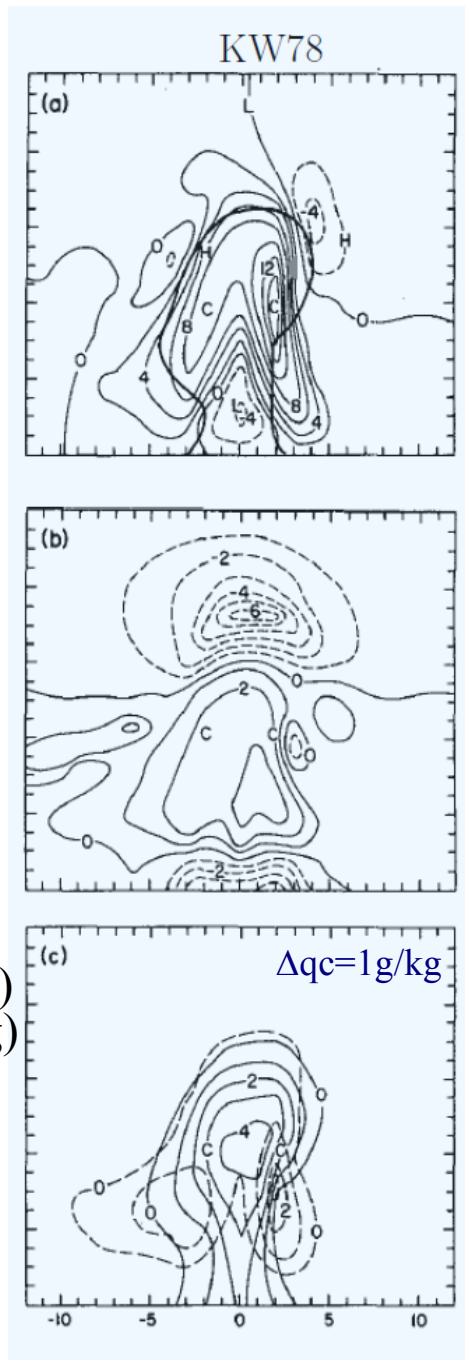
X-Z cross-section
at $y=2\text{ km}$

time=40min

— $w > 0$ (m/s)
 $w < 0$ (m/s)
 — $q_r > 1 \text{ g/kg}$

— $\theta > 0$ (K)
 $\theta < 0$ (K)

— $q_r > 0$ (g/kg)
 $q_c > 0$ (g/kg)

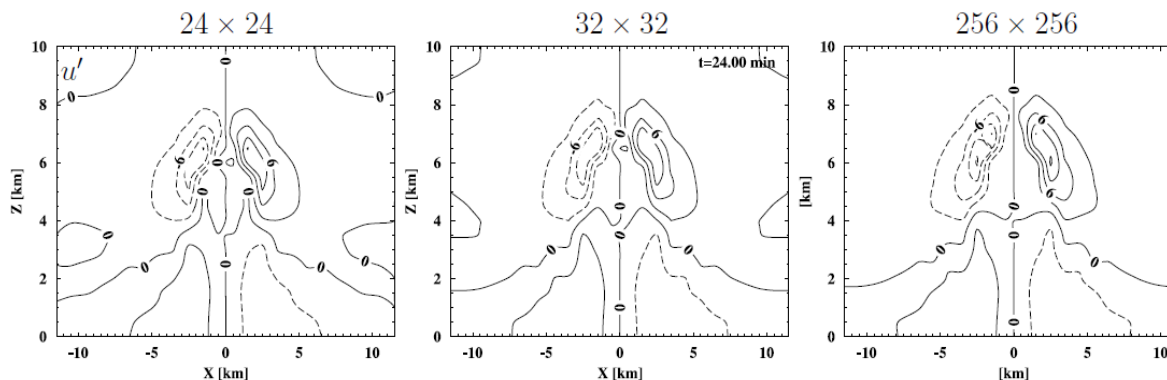


O – open b.c., P – periodic b.c.

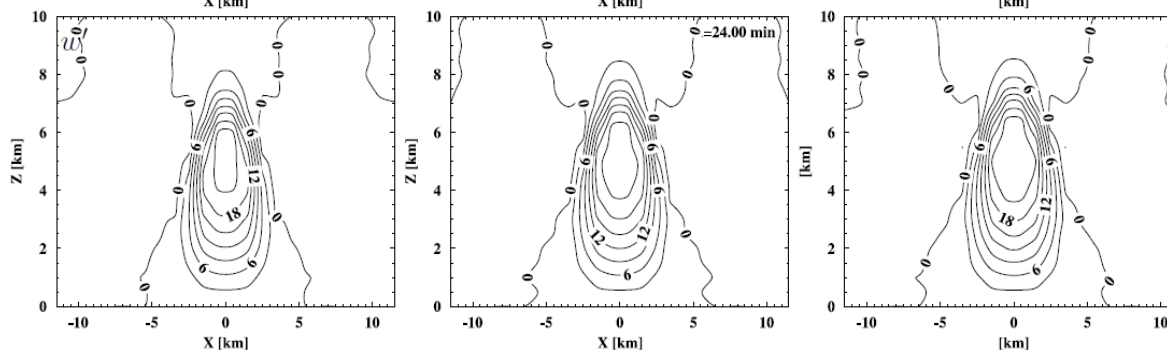
Setup name	u_{max} [m/s]	u_{min} [m/s]	w_{max} [m/s]	w_{min} [m/s]	$q_c \text{ max}$ [g/kg]	$q_r \text{ max}$ [g/kg]	θ'_{max} [K]	θ'_{min} [K]
<i>No Shear</i>								
256x256.P.24min	-11.876	11.876	22.506	-2.812	2.289	7.504	5.772	-3.480
32x32.O.24min	-10.876	10.876	22.270	-2.451	2.287	7.034	5.691	-3.228
32x32.P.24min	-10.877	10.877	22.270	-2.451	2.284	7.034	5.691	-3.228
24x24.O.24min	-11.295	11.295	21.741	-2.253	2.300	6.306	5.595	-3.294
24x24.P.24min	-11.296	11.296	21.742	-2.254	2.300	6.306	5.595	-3.291
<i>With Shear</i>								
256x256.P.24min	-8.636	12.240	17.970	-2.362	2.836	4.283	5.098	-2.741
32x32.O.24min	-8.508	11.744	17.039	-2.590	2.809	3.826	5.001	-2.631
32x32.P.24min	-8.484	11.709	17.001	-2.534	2.805	3.816	5.000	-2.639
24x24.O.24min	-8.254	11.592	15.364	-2.099	2.632	3.132	4.732	-2.265
24x24.P.24min	-8.241	11.451	15.356	-2.172	2.653	3.120	4.736	-2.269
256x256.P.36min	15.791	-10.929	20.568	-8.185	1.561	12.389	5.378	-7.551
32x32.O.36min	15.653	-11.332	19.601	-8.507	1.571	12.182	4.714	-6.352
32x32.P.36min	15.425	-11.212	19.509	-8.472	1.581	12.180	4.741	-6.506
24x24.O.36min	13.072	-11.290	19.728	-7.609	1.113	11.138	4.299	-5.076
24x24.P.36min	12.772	-11.229	19.530	-7.753	1.167	11.163	4.315	-5.105



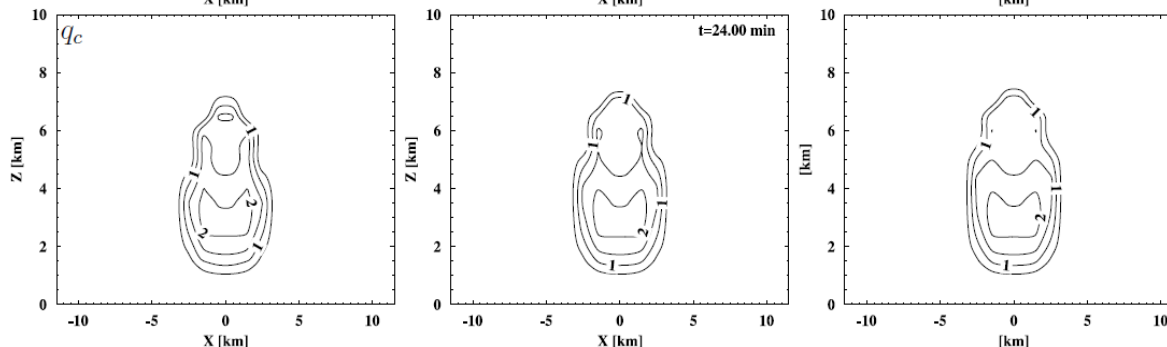
U (m/s)
 $\Delta U = 3 \text{ m/s}$



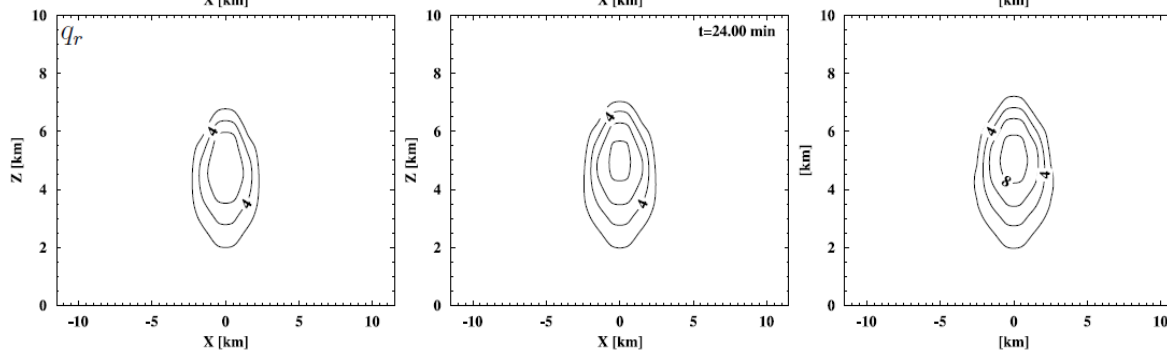
W (m/s)
 $\Delta W = 3 \text{ m/s}$



q_c (g/kg)
 $\Delta q_c = 0.5 \text{ g/kg}$



q_r (g/kg)
 $\Delta q_r = 2 \text{ g/kg}$



Domain size is
different but grid
spacing is fixed.



Summary of KW78 experiment:

- Dynamical fields are in good agreement with KW78 results for unsheared environment, shear flow and veering wind;
- Influence of boundary conditions is negligible, especially for large horizontal domain size;
- The solution is strongly influenced by the subgrid-scale mixing;
- Most significant difference concerns the moist fields: EULAG's simulations seem to produce lower amount of cloud and rain mixing ratio;



**The Dependence of Numerically Simulated Convective Storms
on Vertical Wind Shear and Buoyancy**

M. L. WEISMAN AND J. B. KLEMP

National Center for Atmospheric Research,¹ Boulder, CO 80307

(Manuscript received 9 October 1981, in final form 2 February 1982)



Grid: uniform (WK82 uses stretched grid),

$dx=dy=2\text{km}$, $dz=350\text{m}$

domain size: $128 \times 128 \times 17.5 \text{ km}$

Subgrid-scale processes:

1) TKE scheme, $Pr=0.33$

2) ILES (implicit large-eddy simulation)

Moist processes:

bulk parametrization, Kessler scheme

Boundary conditions:

open b.c. (additionally periodic)

Initial conditions:

realistic sounding

Integration time:

120 min

Setup details agreed with WK82



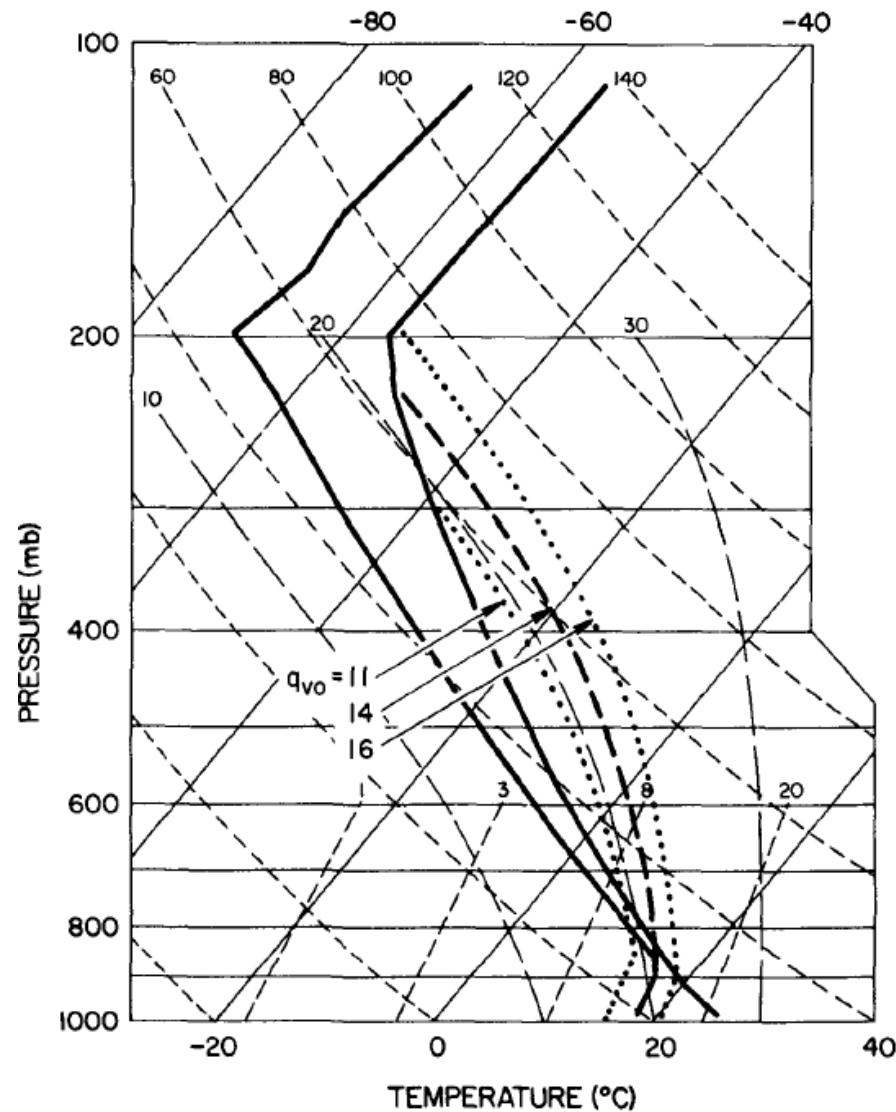
Analytic profiles of potential
temperature and relative humidity

$$\bar{\theta}(z) = \begin{cases} \theta_0 + (\theta_{tr} - \theta_0) \left(\frac{z}{z_{tr}} \right)^{5/4}, & z \leq z_{tr} \\ \theta_{tr} \exp \left[\frac{g}{c_p T_{tr}} (z - z_{tr}) \right], & z > z_{tr} \end{cases}$$

$$H(z) = \begin{cases} 1 - \frac{3}{4} \left(\frac{z}{z_{tr}} \right)^{5/4}, & z \leq z_{tr} \\ 0.25, & z > z_{tr} \end{cases}$$

$$z_{tr} = 12 \text{ km}, \theta_{tr} = 343 \text{ K and } T_{tr} = 213 \text{ K}$$

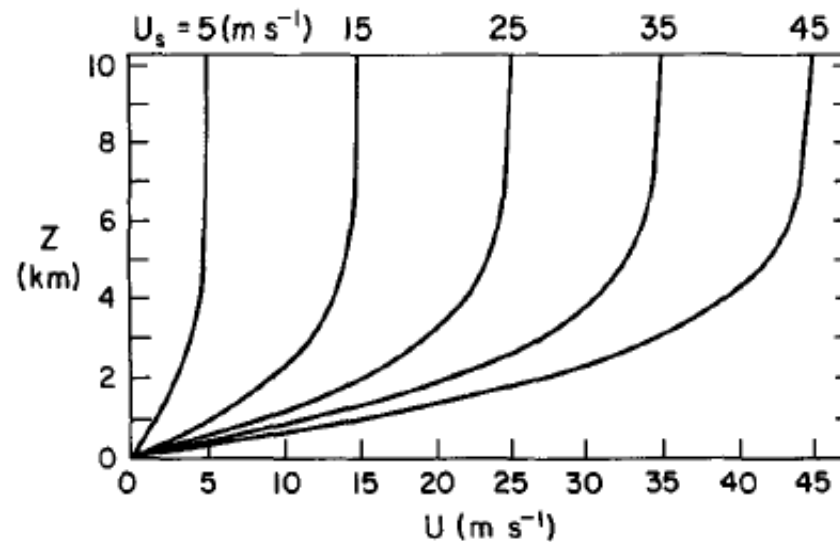
$$\theta_0 = 300 \text{ K}$$

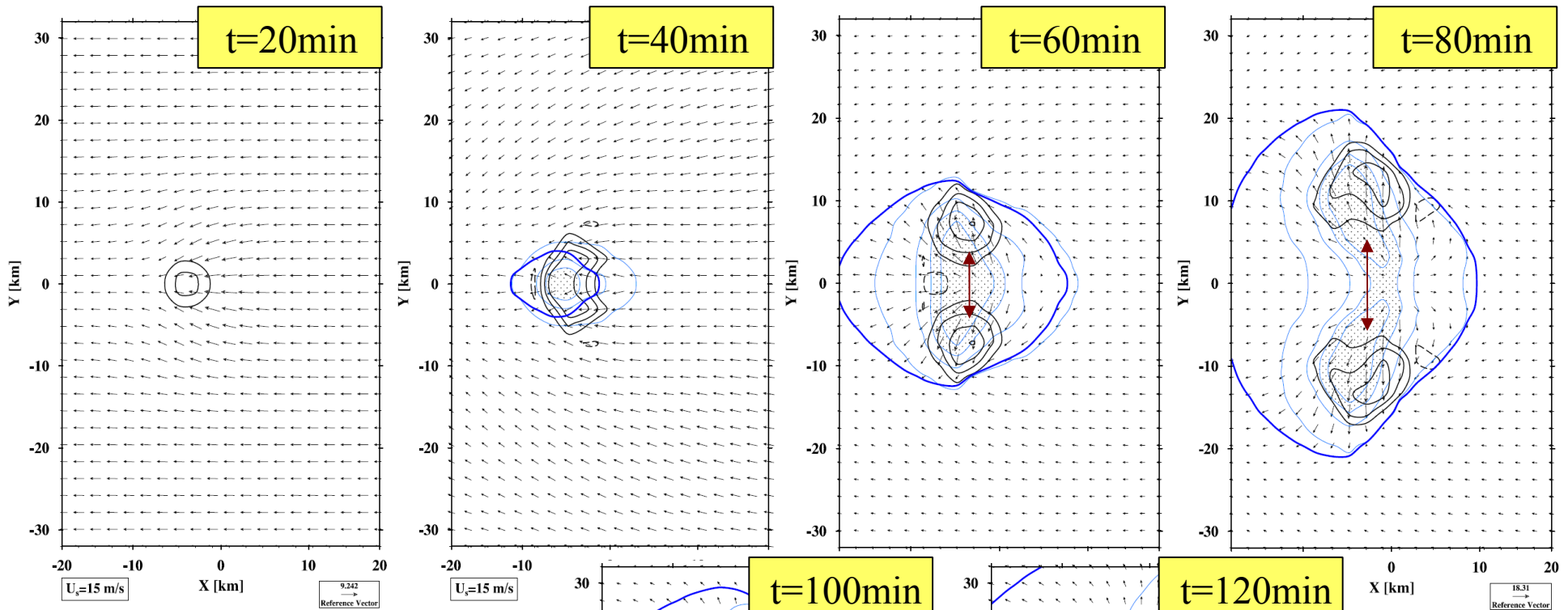


Horizontal velocity profile in x-direction
(analytic)

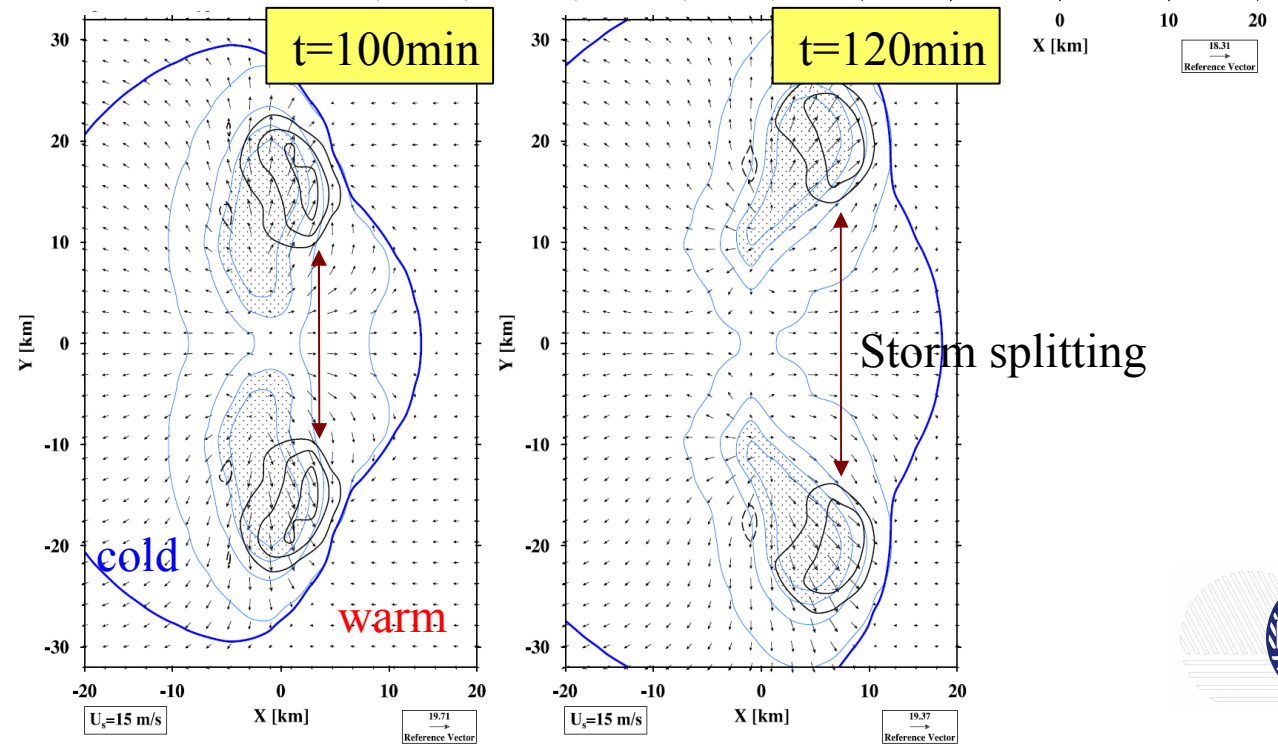
$$U = U_S \tanh z / z_s$$

$$z_s = 3 \text{ km}$$



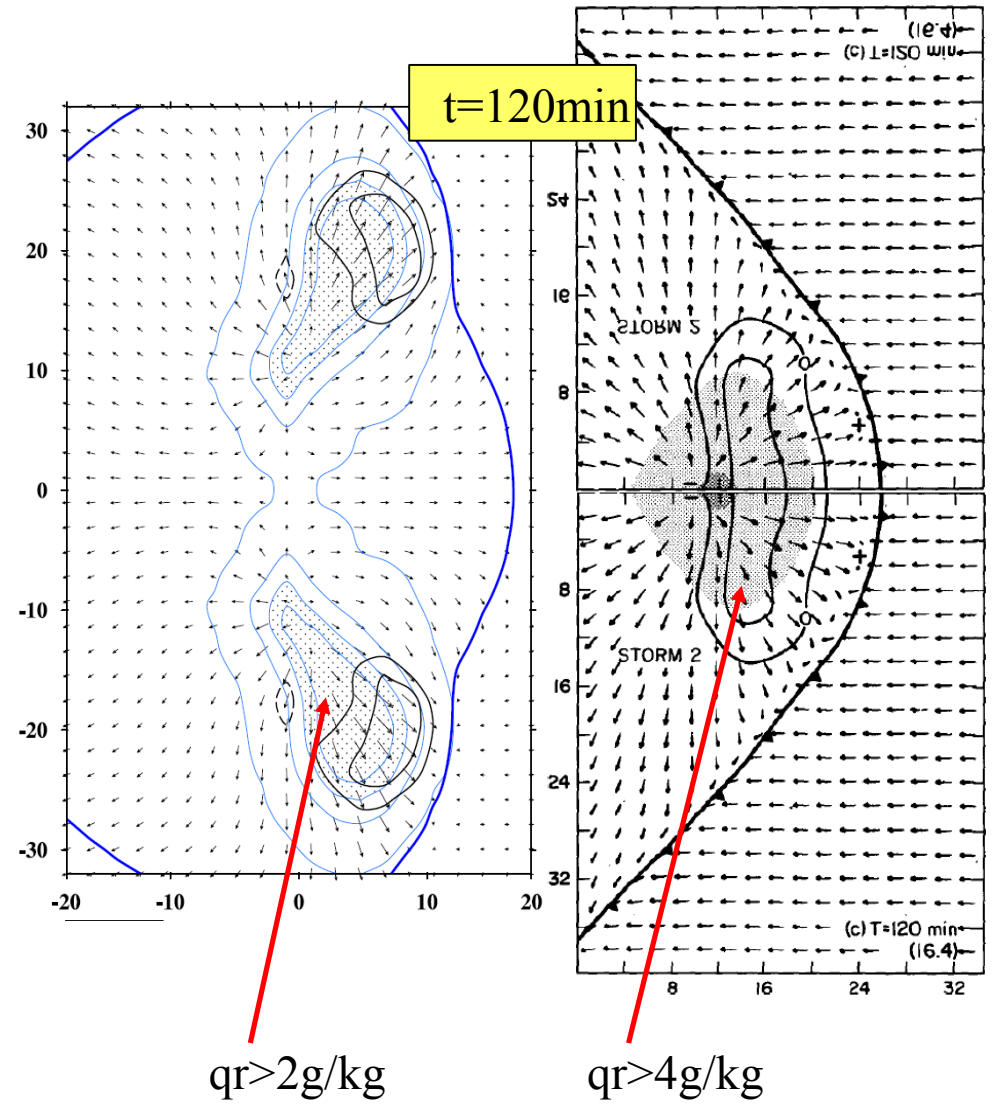
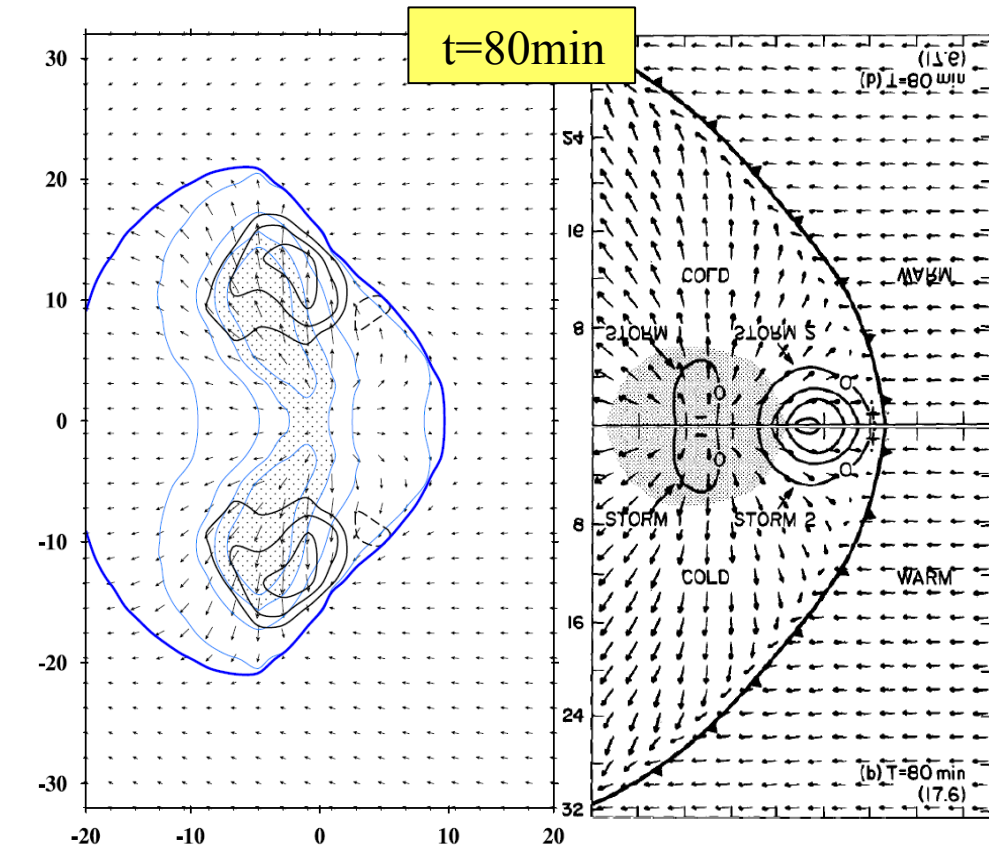
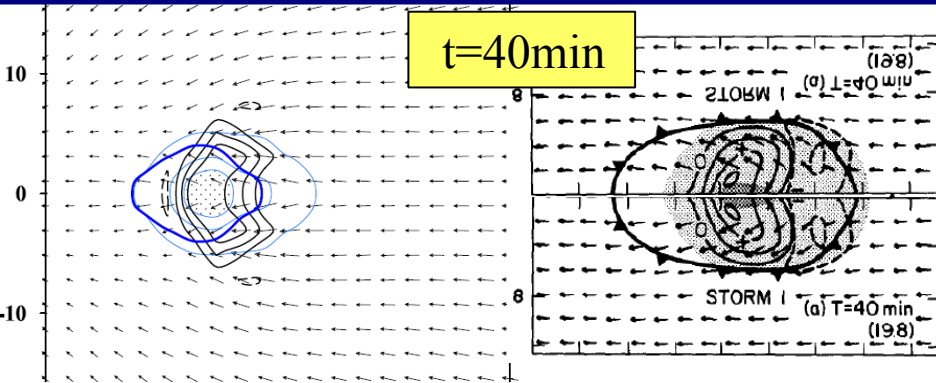


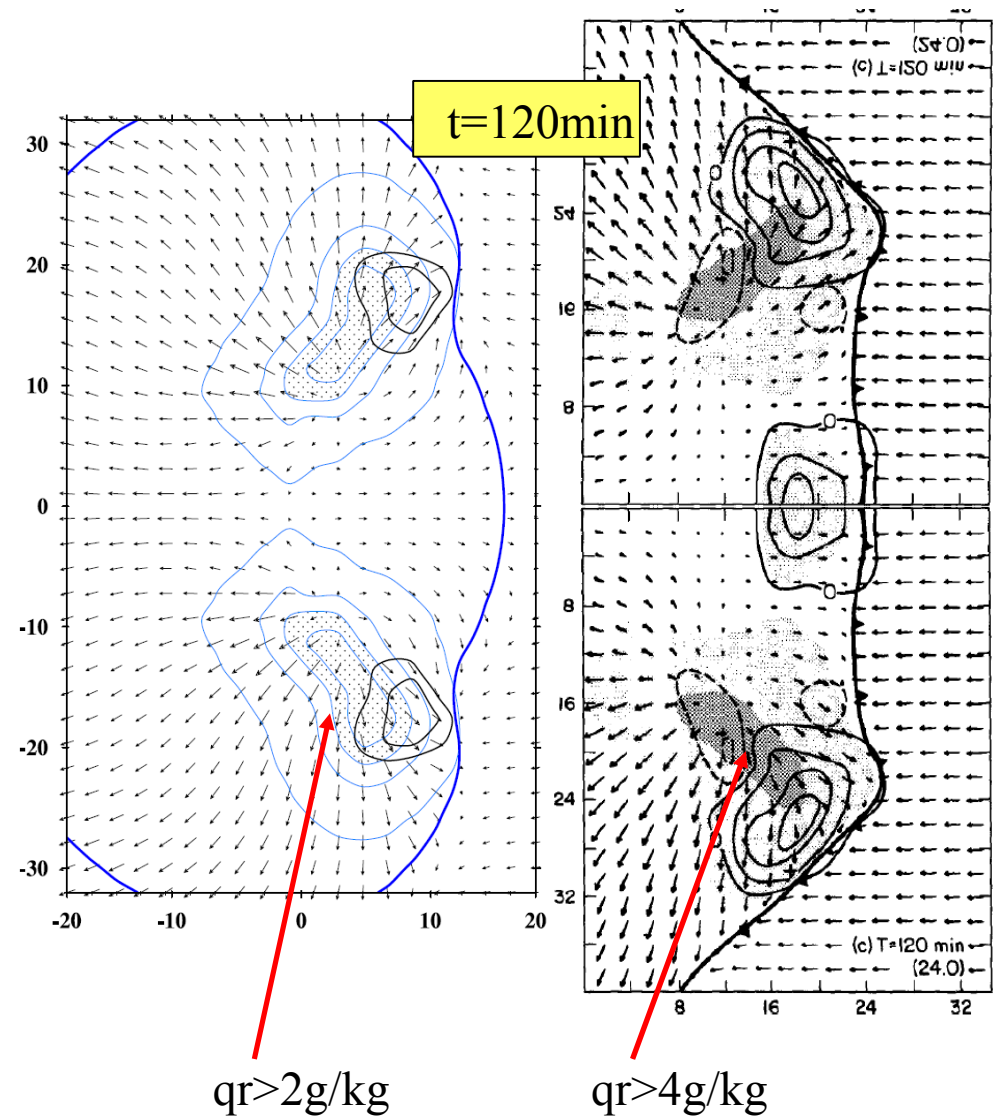
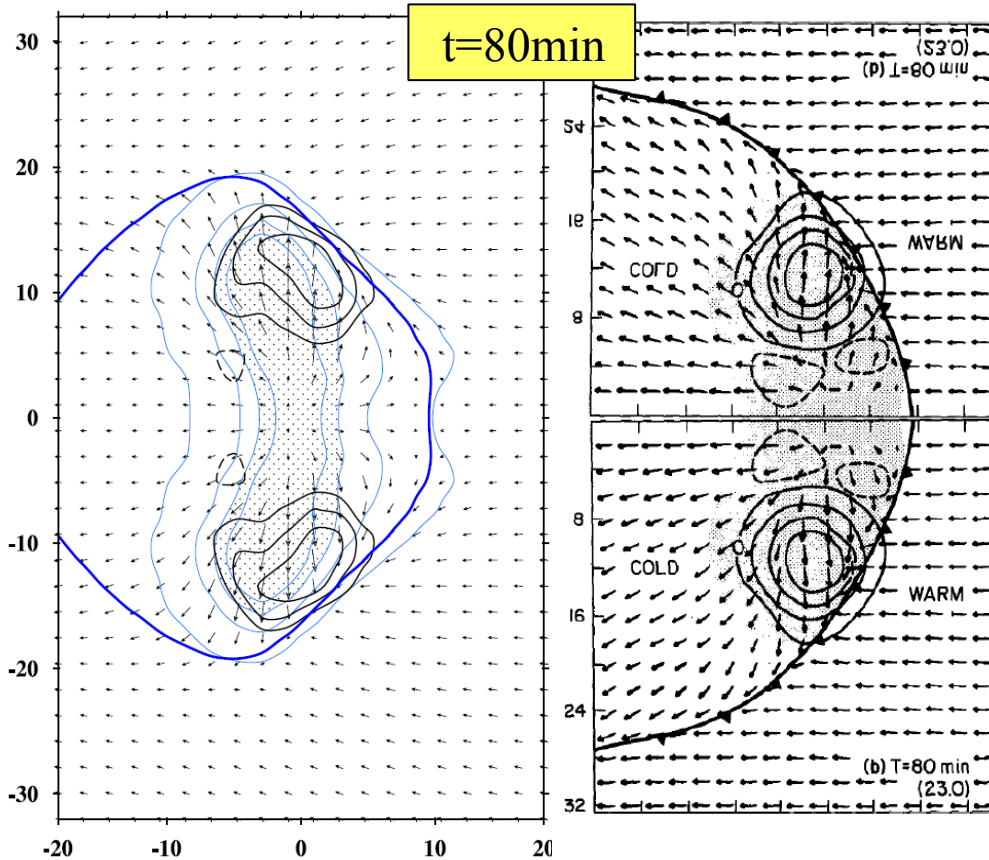
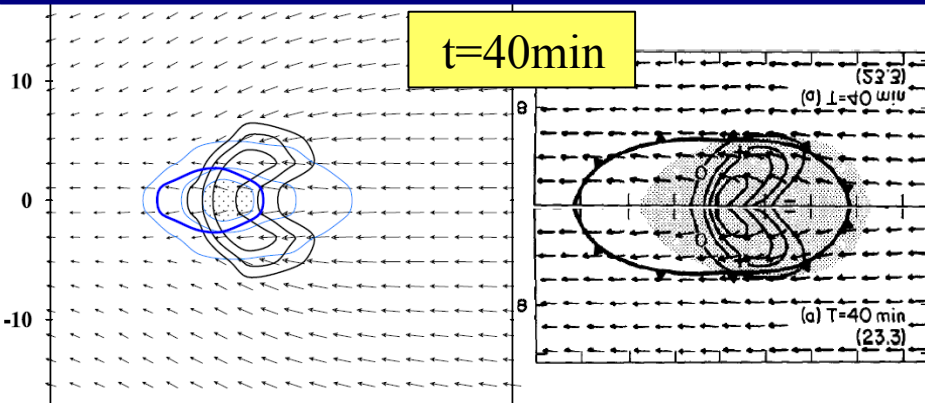
- cold front ($\theta' = -0.5\text{K}$) at the surface
- qr at $z=175\text{m}$
 $\Delta q_r = 1\text{g/kg}$
- $w > 0$ at $z=5\text{km}$
 $\Delta w = 5\text{m/s}$
- $w < 0$ at $z=5\text{km}$
 $\Delta w = -2\text{m/s}$
- ← (u, v) at $z=350\text{m}$

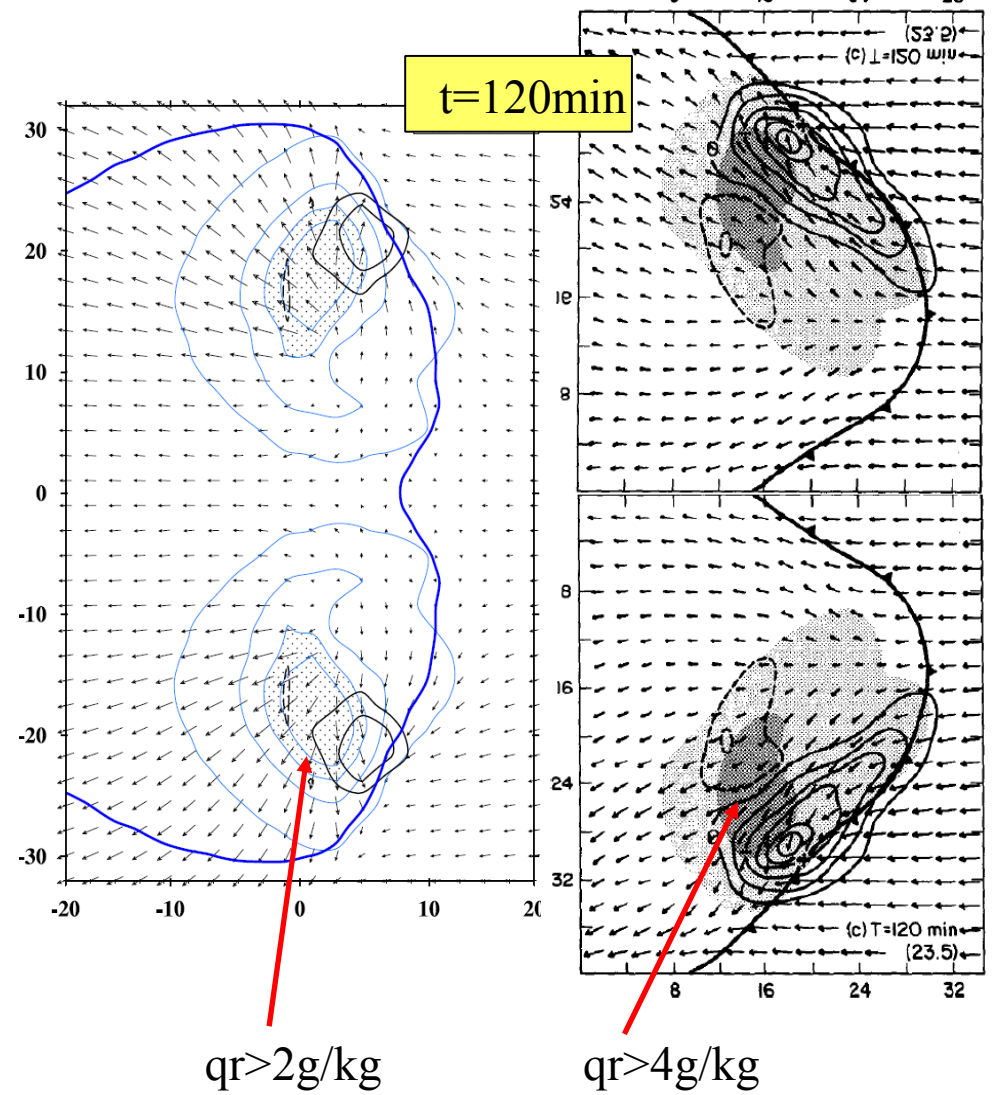
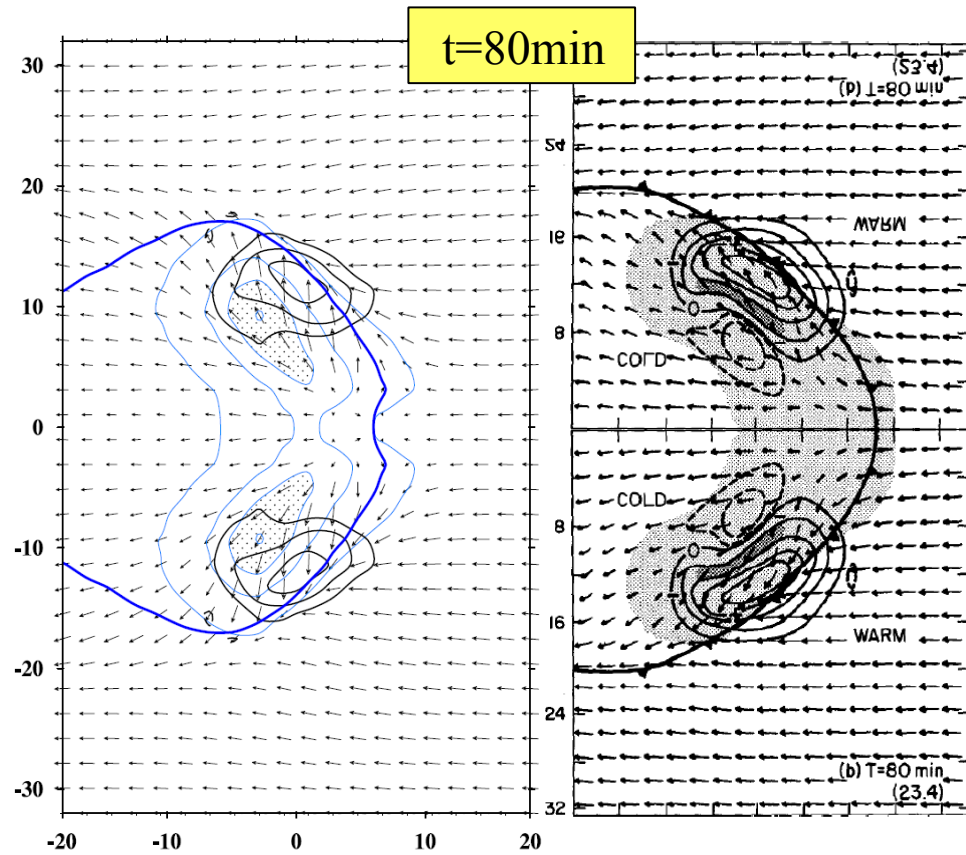
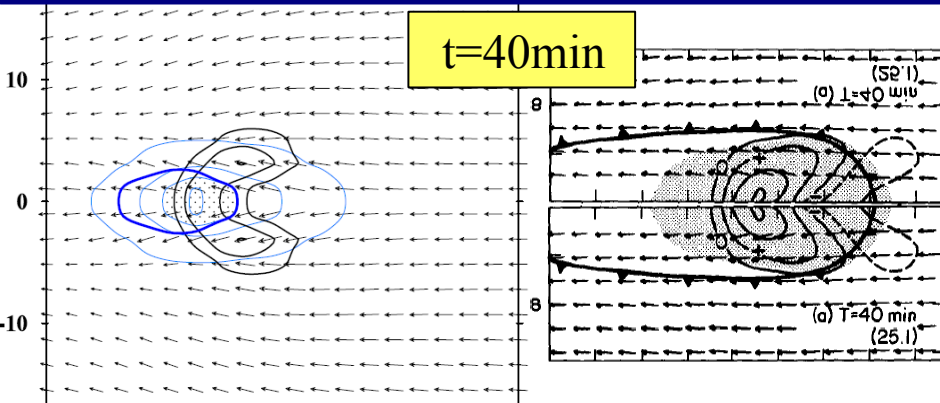


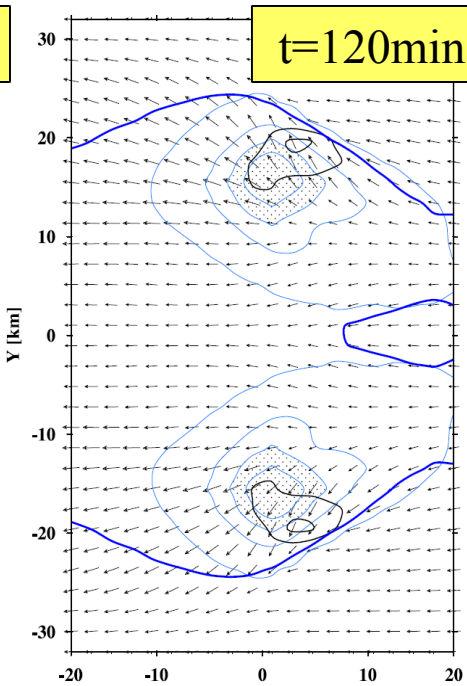
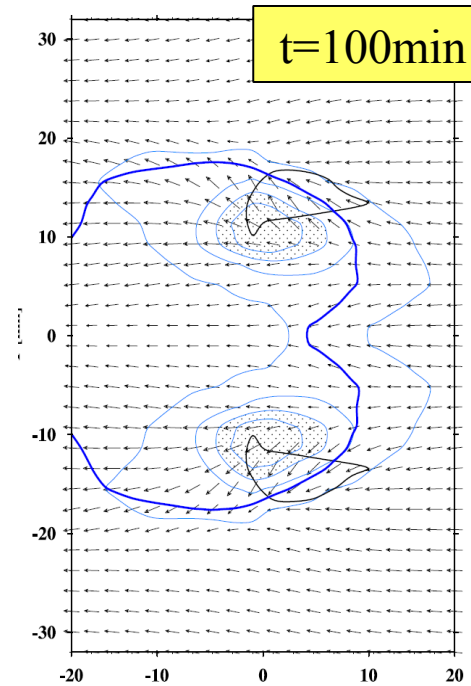
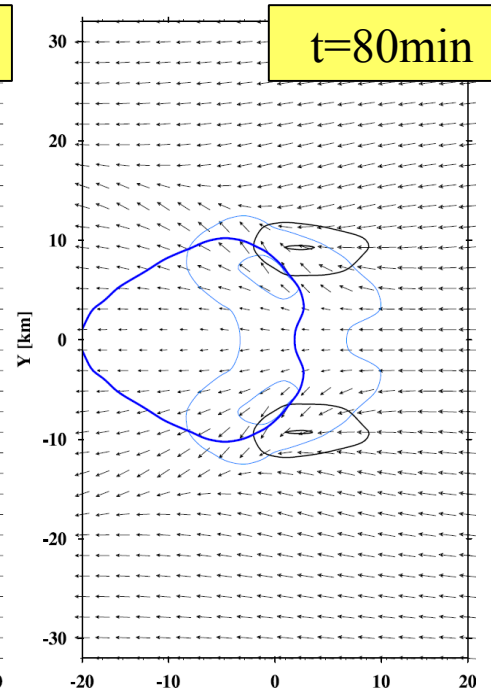
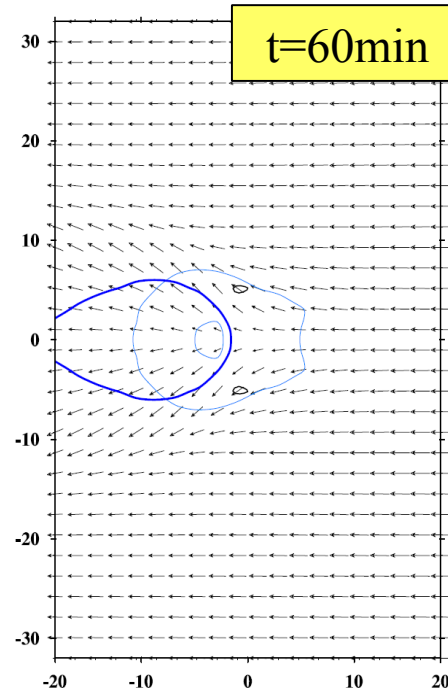
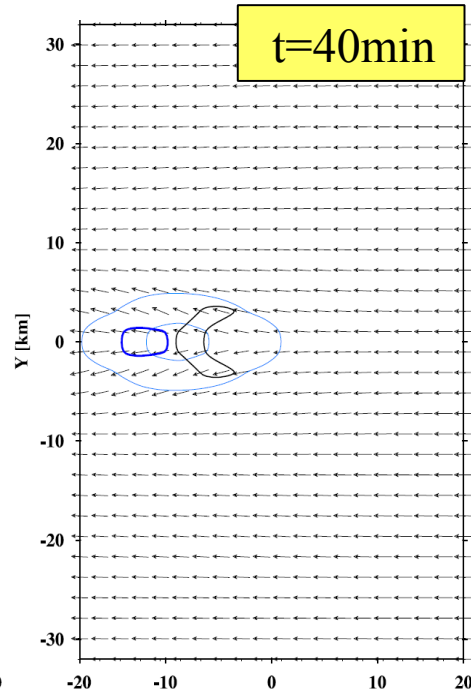
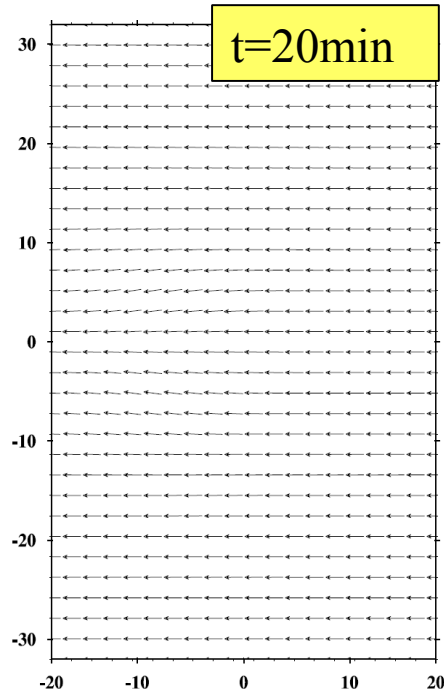
Storm splitting

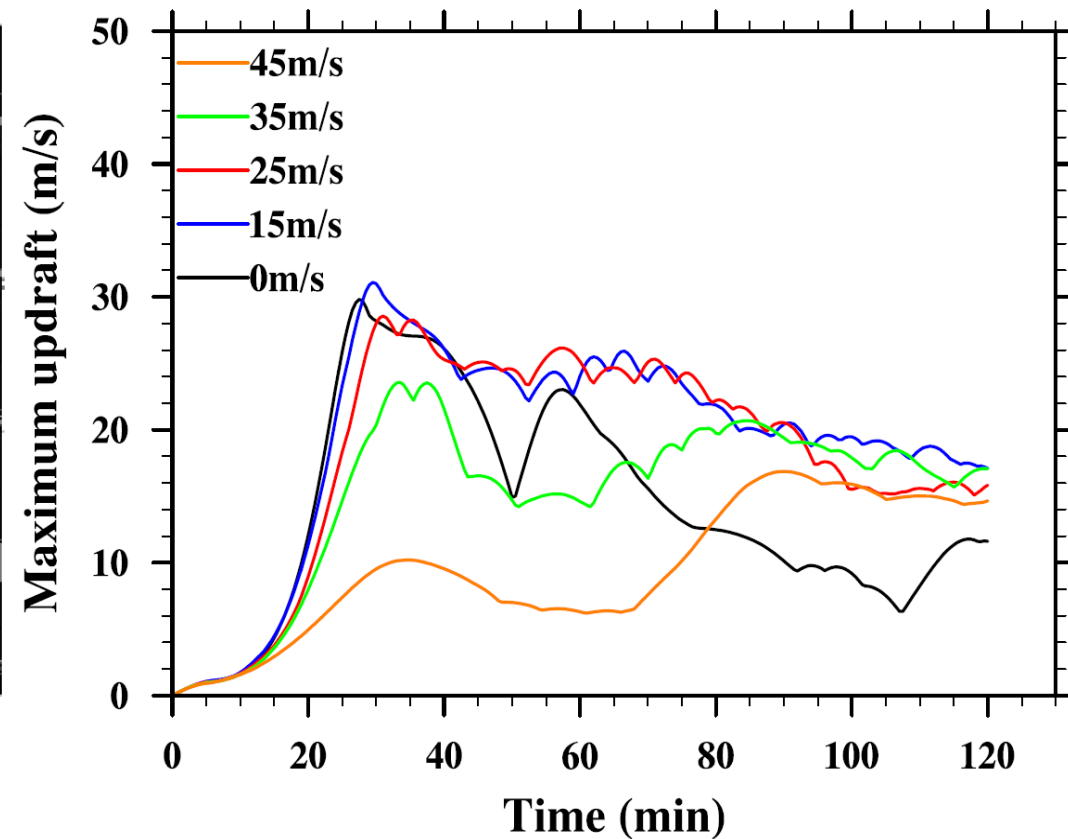
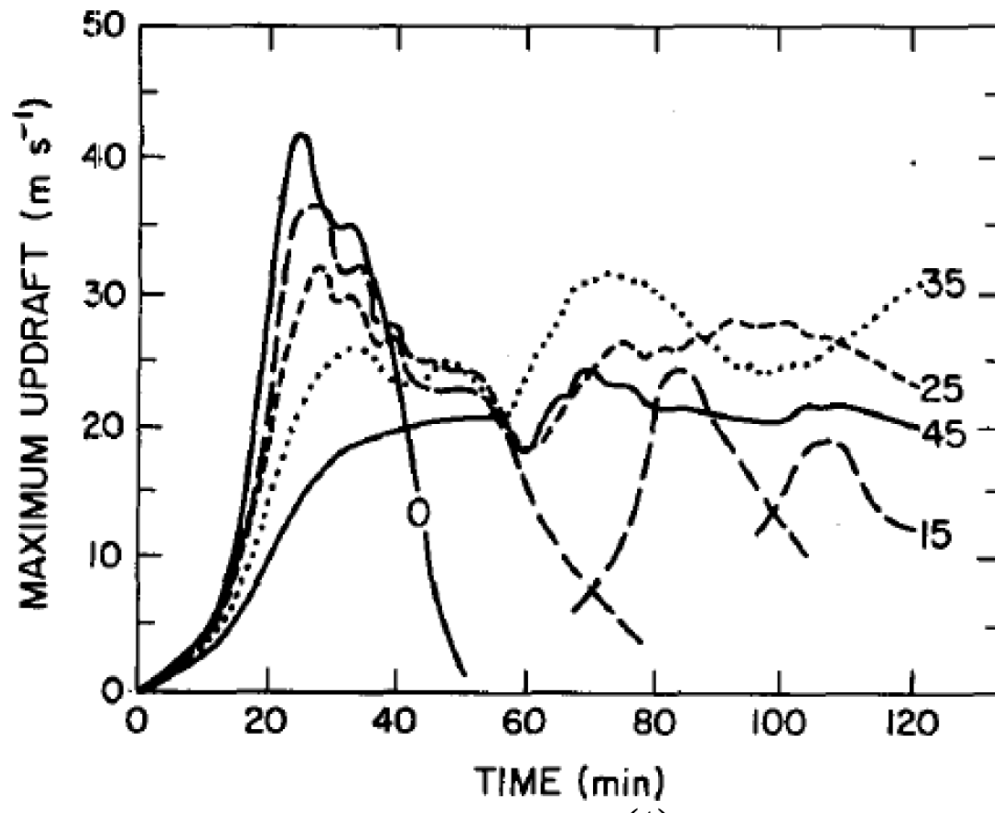












Supercell behaviour \Leftrightarrow quasi-steady updraft

No shear \rightarrow dies first
Larger shear \rightarrow weaker development



Summary of moist experiments:

- Realistic reconstruction of storm splitting
- Similar shape and time evolution of cloud/rain fields and cold pool formation
- Storm splitting is observed for weaker shear flow
- All numerical solutions are in qualitative agreement, but with less vigorous dynamics and lower amount of cloudy/rain water

