

The Fluid Dynamics of Tornadoes

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NCAR

Lecture 3: Numerical Simulations & Dynamics of The Two-Celled Vortex



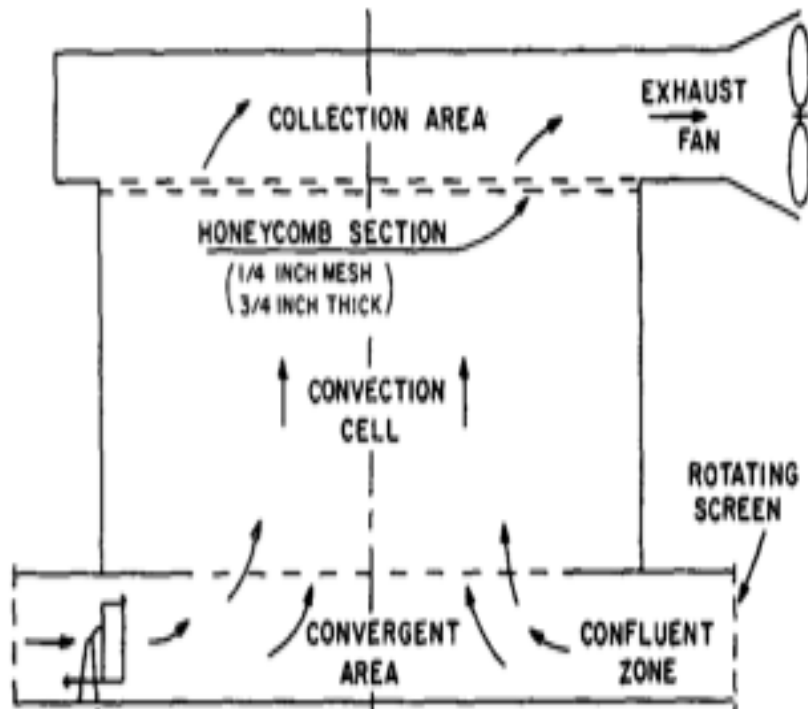
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NCAR is funded by the National Science Foundation



Numerical Model of Ward Vortex Chamber

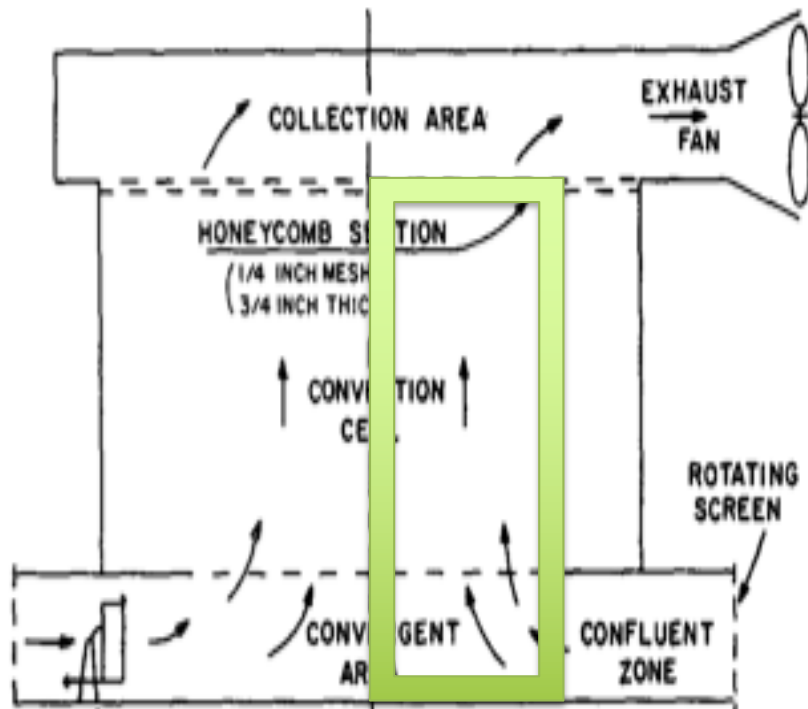
...inadequate top boundary condition... → ...difficult to model top boundary condition...



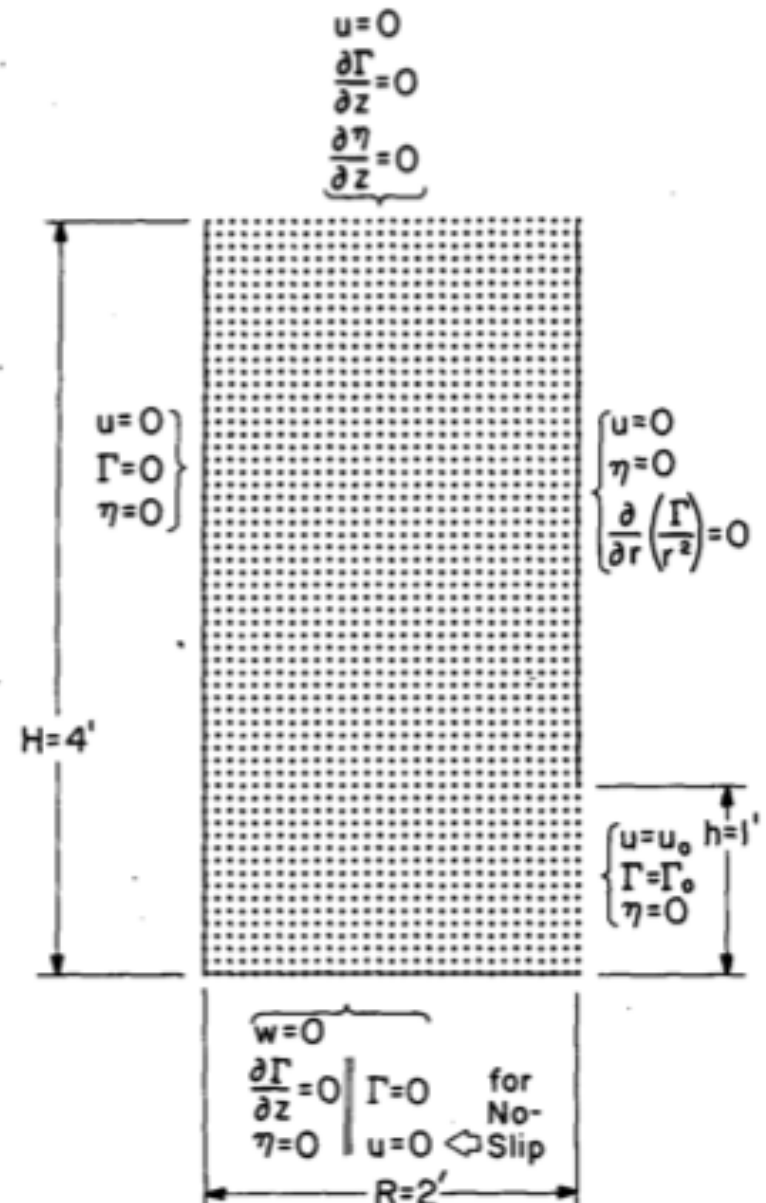
Ward (1972, JAS)

Numerical Model of Ward Vortex Chamber

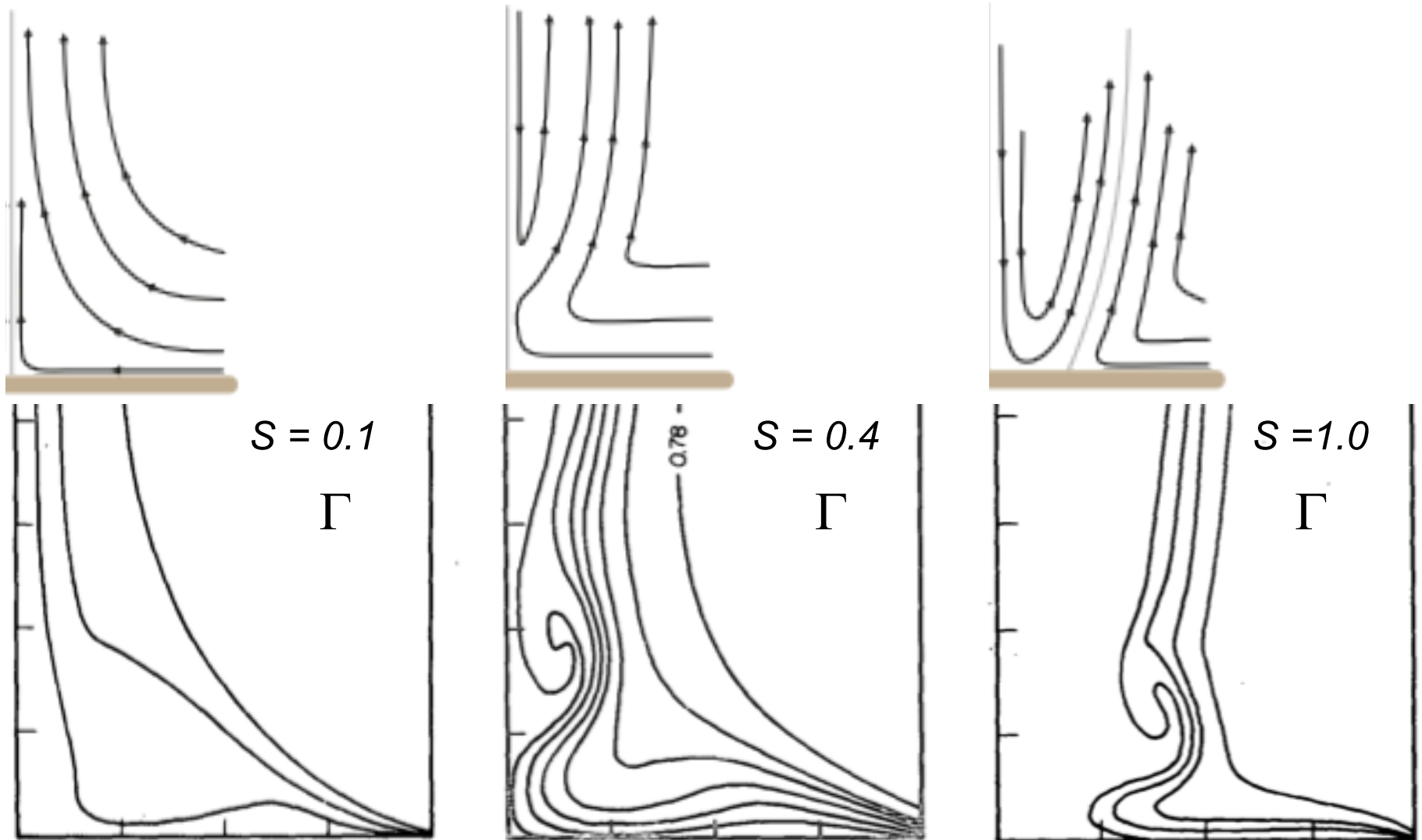
...inadequate top boundary condition... → ...difficult to model top boundary condition...



Rotunno (1977, JAS)



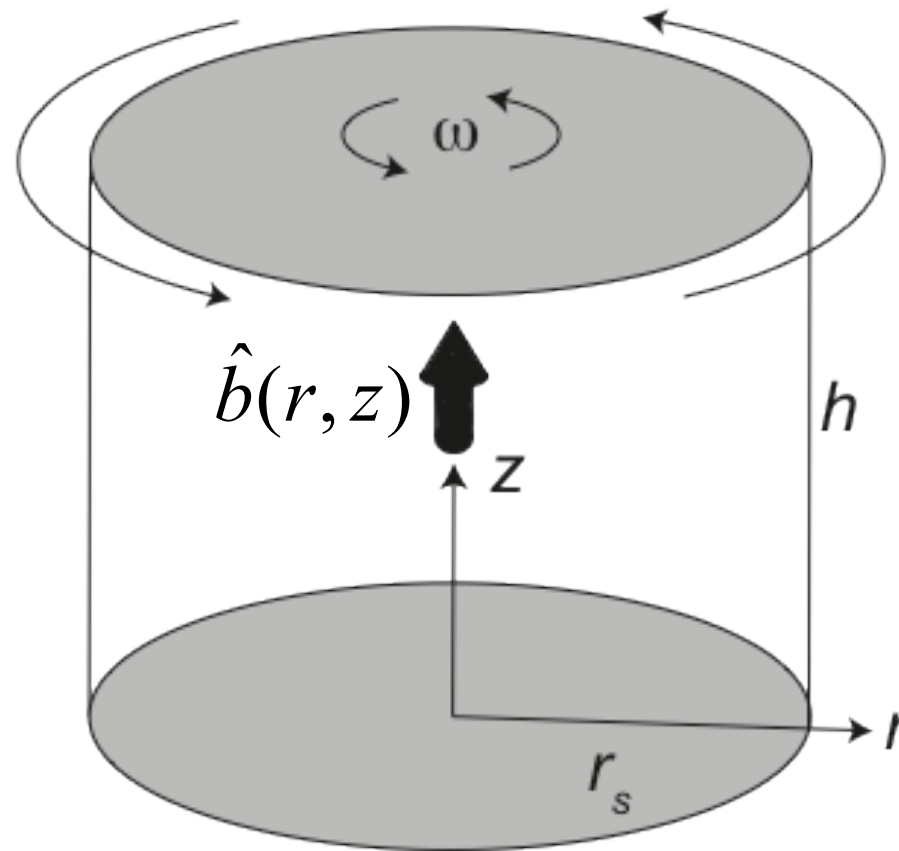
Numerical Simulations of Ward Chamber



Rotunno (1979, *JAS*)

Fiedler Chamber

Boundary condition
 $[u, v, w] = 0$



$$\Omega = \frac{\omega h}{W}$$

Swirl Ratio

$$N = \frac{Wh}{\nu}$$

Reynolds #

$$W \equiv \sqrt{2 \int_0^h \hat{b}(0, z) dz}$$

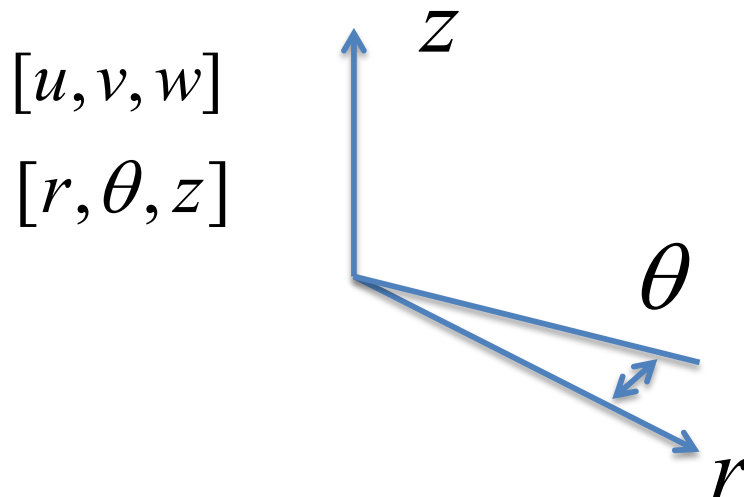
Nondimensional Governing Equations in Cylindrical Polar Coordinates

$$\frac{du}{dt} = -\frac{\partial p}{\partial r} + \frac{v^2}{r} + 2\Omega v + \frac{1}{N} \left(\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial}{\partial r} (ru) \right) + \frac{\partial^2 u}{\partial z^2} \right)$$

$$\frac{dv}{dt} = -\frac{uv}{r} - 2\Omega u + \frac{1}{N} \left(\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial}{\partial r} (rv) \right) + \frac{\partial^2 v}{\partial z^2} \right)$$

$$\frac{dw}{dt} = -\frac{\partial p}{\partial z} + b + \frac{1}{N} \left(\frac{\partial}{\partial r} \left(r \frac{\partial w}{\partial r} \right) + \frac{\partial^2 w}{\partial z^2} \right)$$

$$\frac{1}{r} \frac{\partial ru}{\partial r} + \frac{\partial w}{\partial z} = 0$$



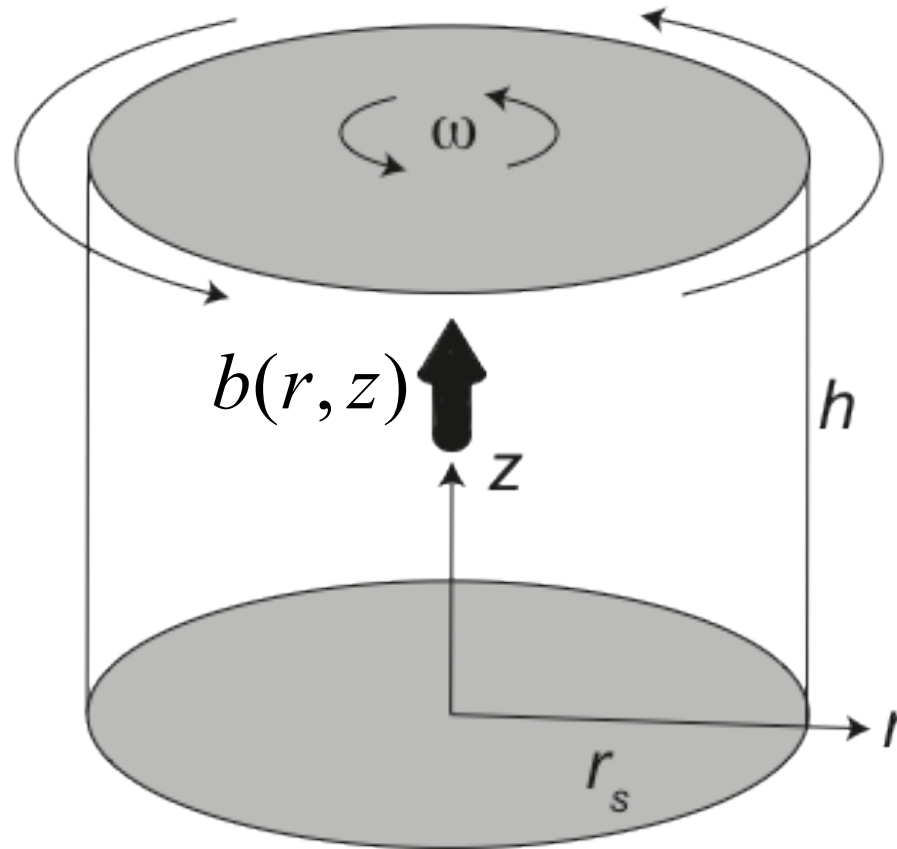
$$W \equiv \sqrt{\frac{\text{velocity scale}}{\text{length scale}}} = \sqrt{2 \int_0^h \hat{b}(0, z) dz} \cong 50 \text{ m/s}$$

$$h \approx 10,000 \text{ m}$$

$$b_o \approx .125 \text{ m/s}^2 \Leftrightarrow \text{Ave. Cell Temp.} \approx 3.75^\circ$$

Fiedler Chamber

Boundary condition
 $[u, v, w] = 0$



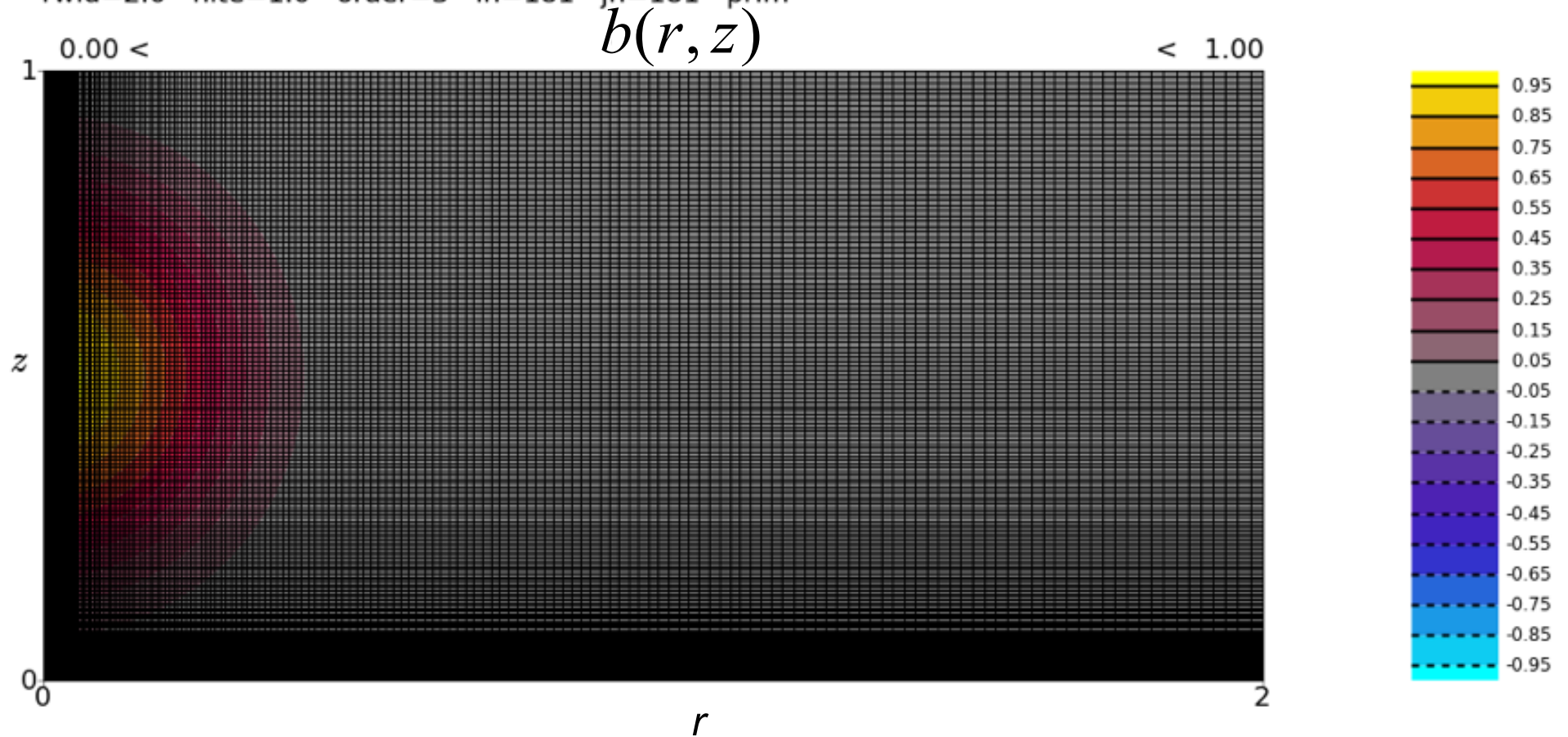
Buoyancy force

$$b(r, z) = 0.5[1 + \cos(2\pi r_b)] \quad \text{for } r_b = \sqrt{r^2 + (z - 0.5)^2} \leq 0.5$$

$$b(r, z) = 0 \quad \text{otherwise}$$

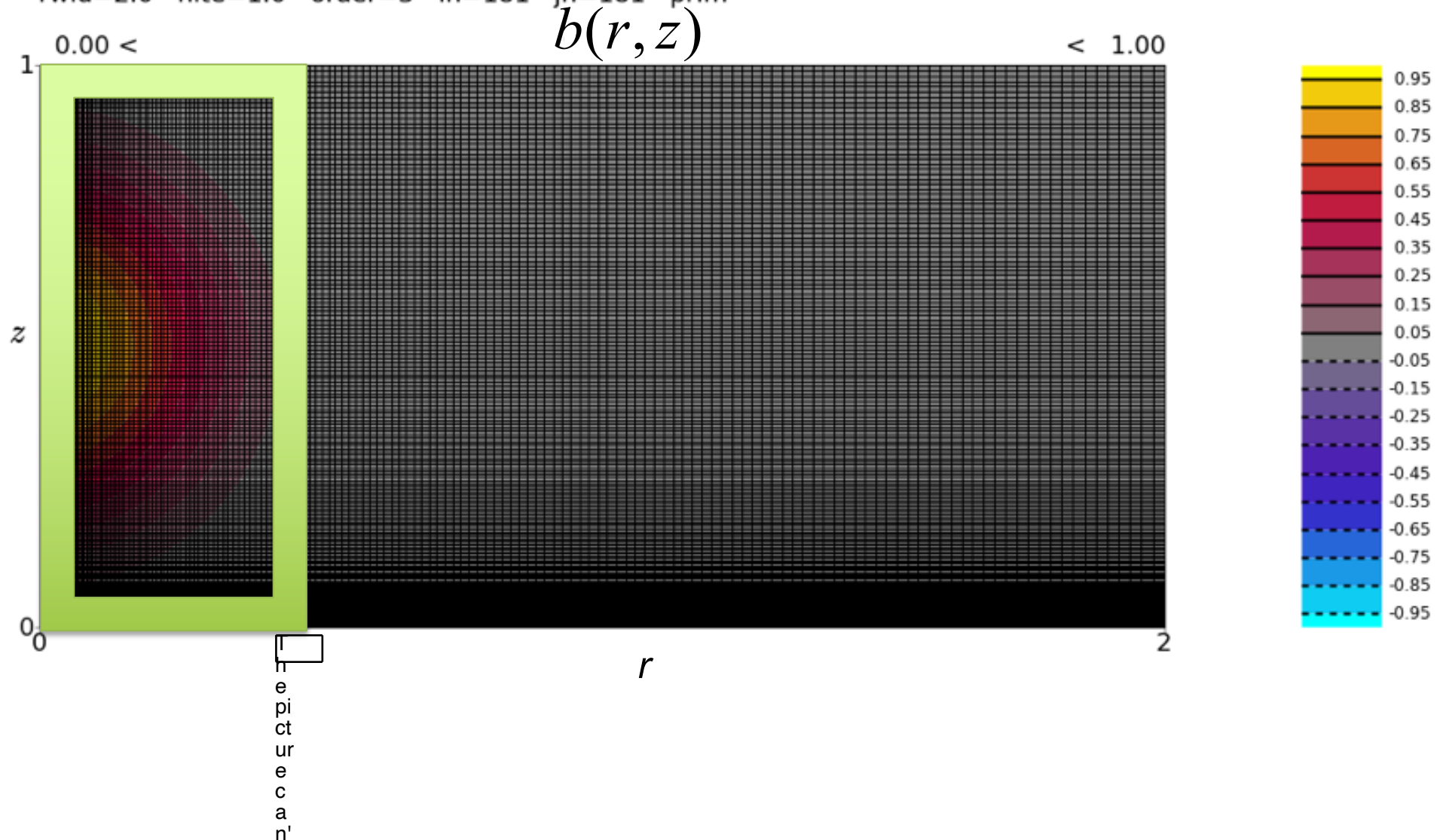
Imposed Buoyancy Force and Grid

time=150.00 rei= 1.00e-04 reit= 1.00e-03 swirl= 5.00e-02
rwid=2.0 hite=1.0 order=3 in=181 jn=181 prim



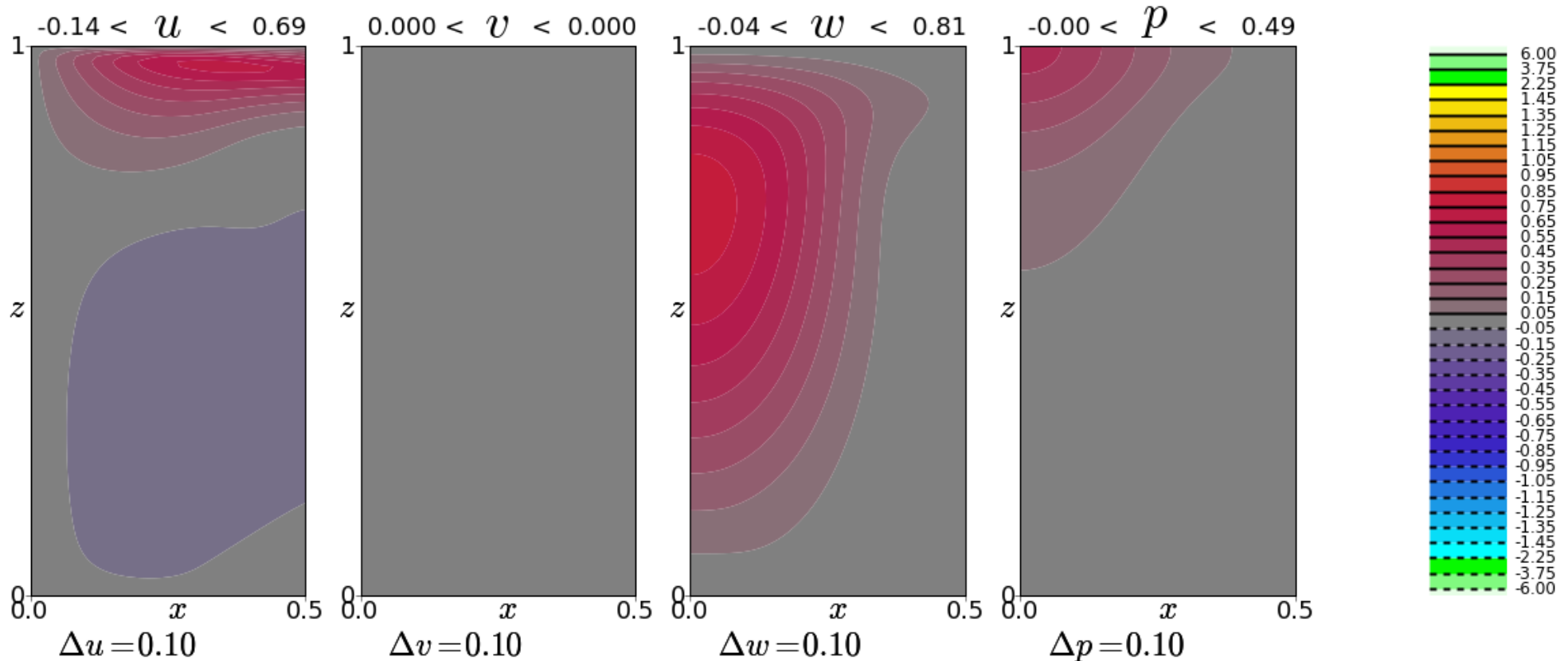
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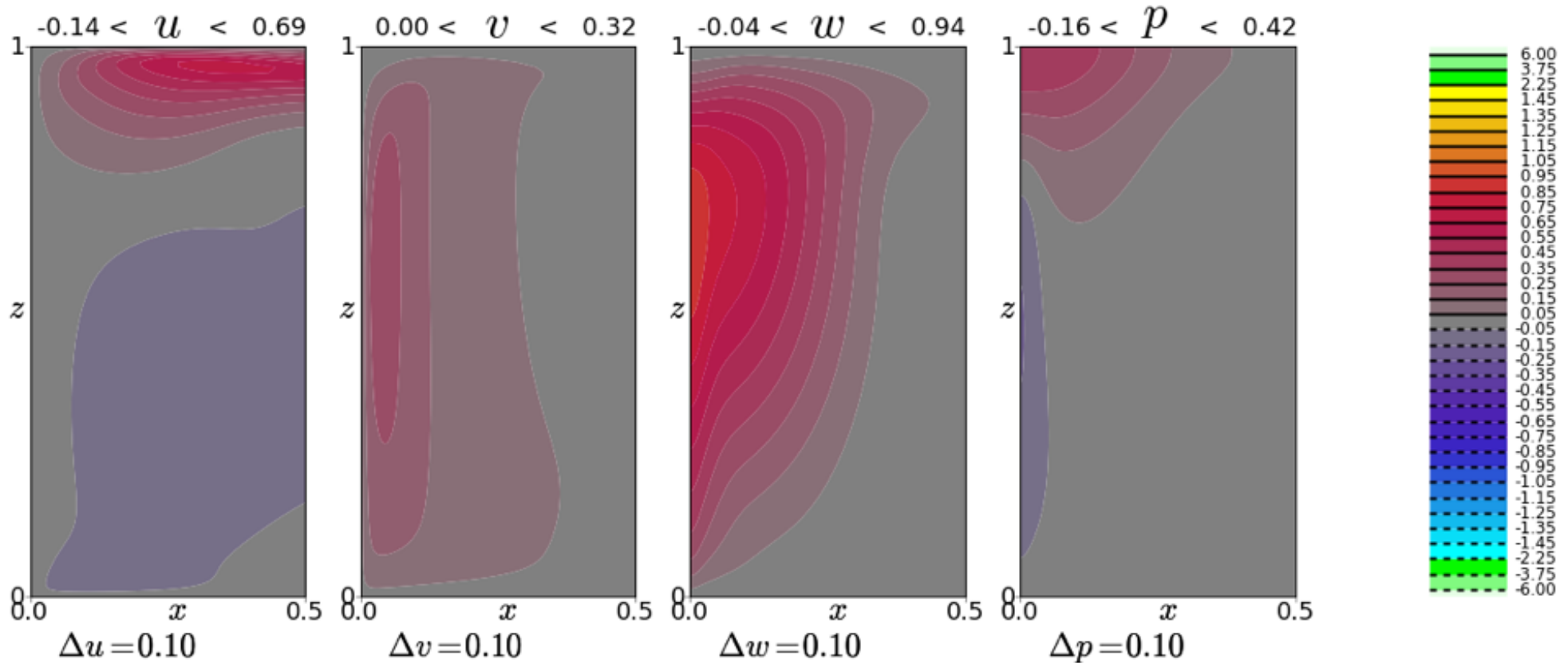
Steady Solution v. Swirl Ratio

time=150.00 rei= 1.00e-04 reit= 1.00e-03 swirl= 0.00e+00
rwid=2.0 hite=1.0 order=3 in=181 jn=181 prim



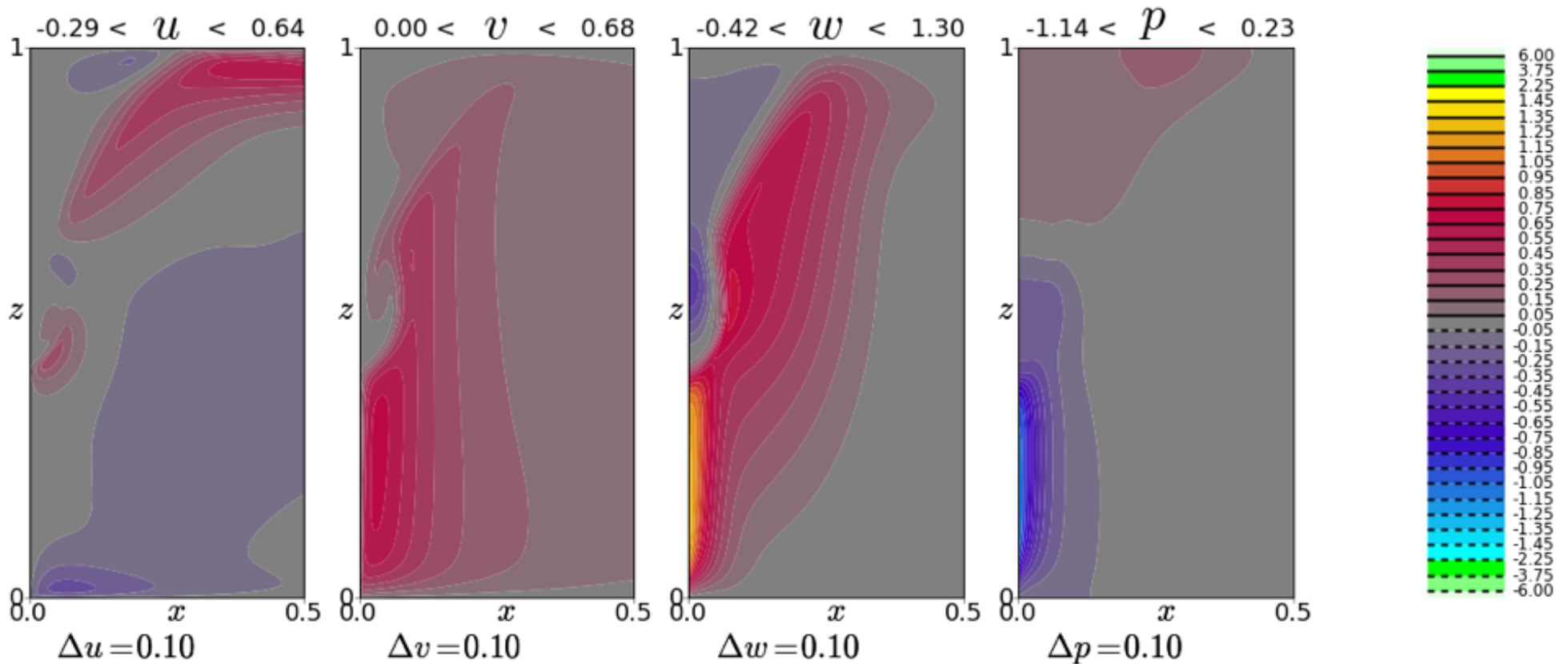
Steady Solution v. Swirl Ratio

time=150.00 rei= 1.00e-04 reit= 1.00e-03 swirl= 2.00e-02
rwid=2.0 hite=1.0 order=3 in=181 jn=181 prim



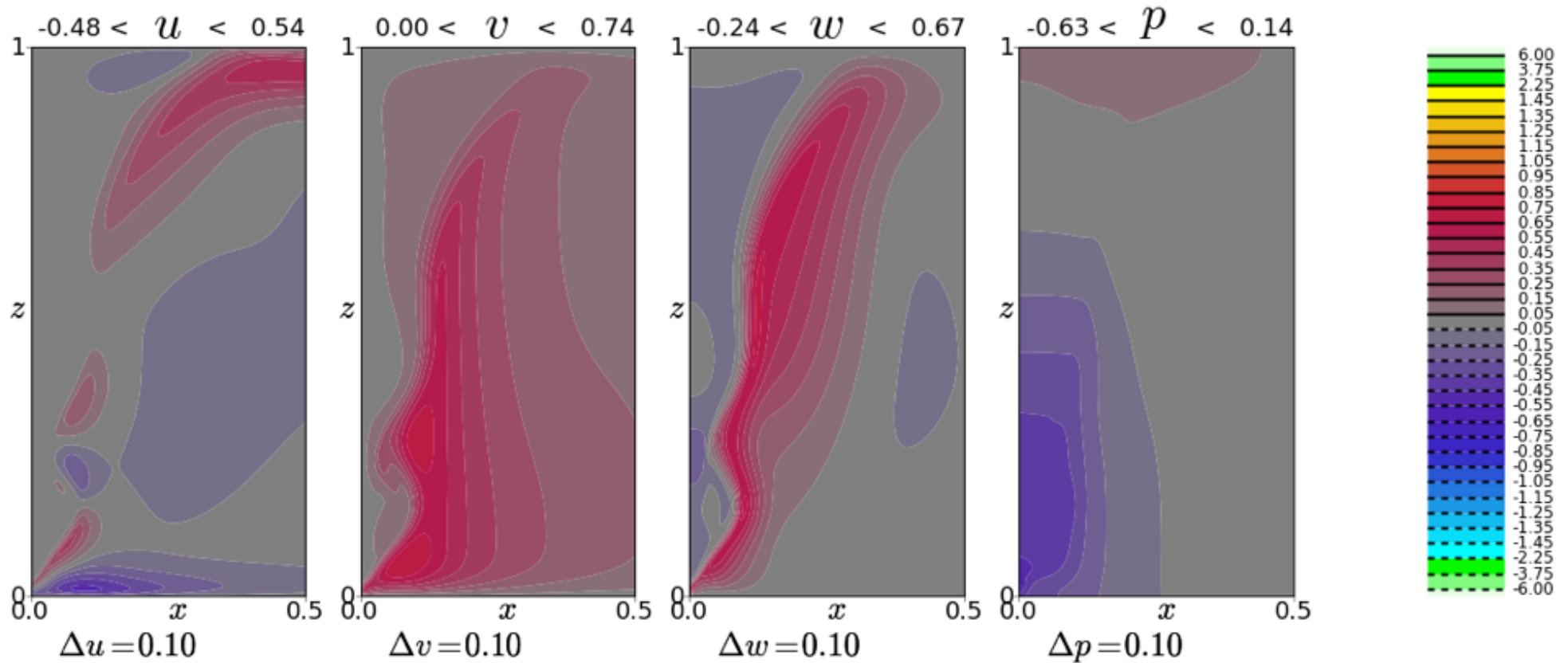
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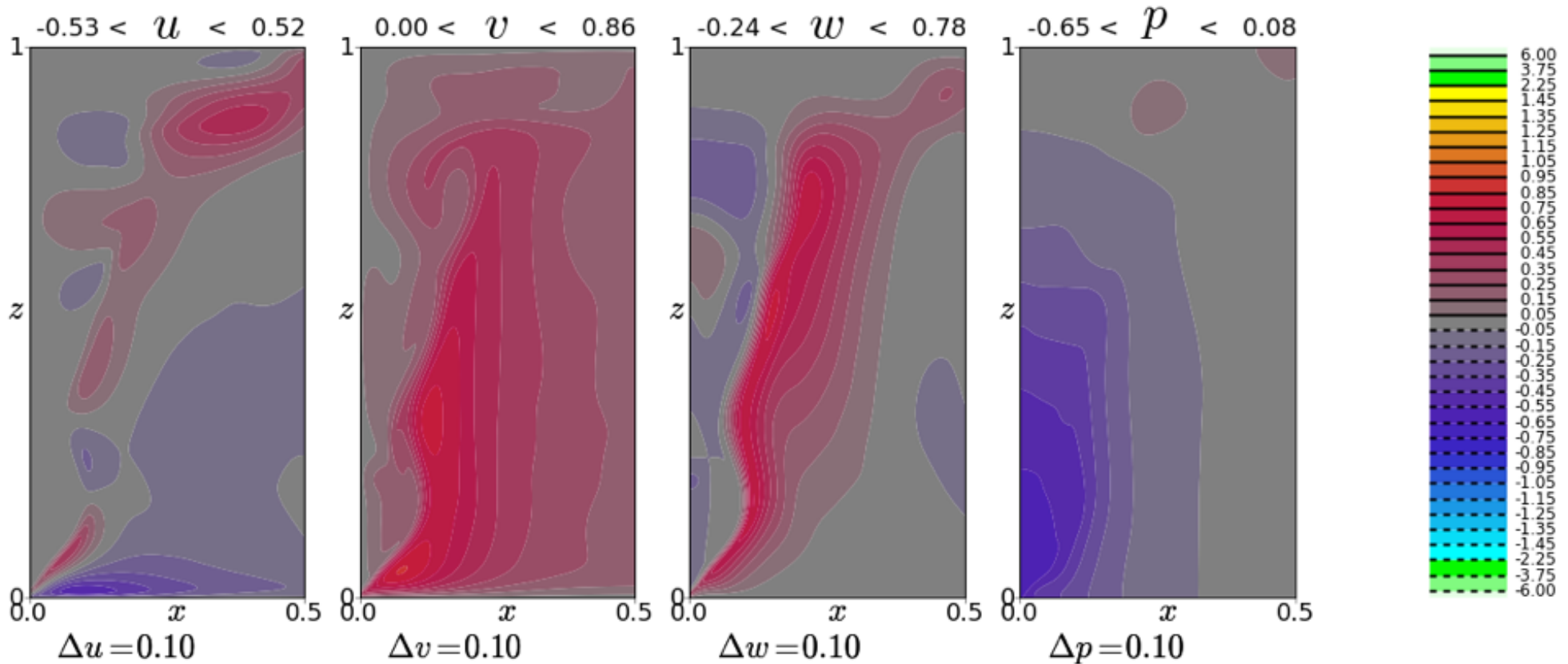
Steady Solution v. Swirl Ratio

time=150.00 rei= 1.00e-04 reit= 1.00e-03 swirl= 1.00e-01
rwid=2.0 hite=1.0 order=3 in=181 jn=181 prim

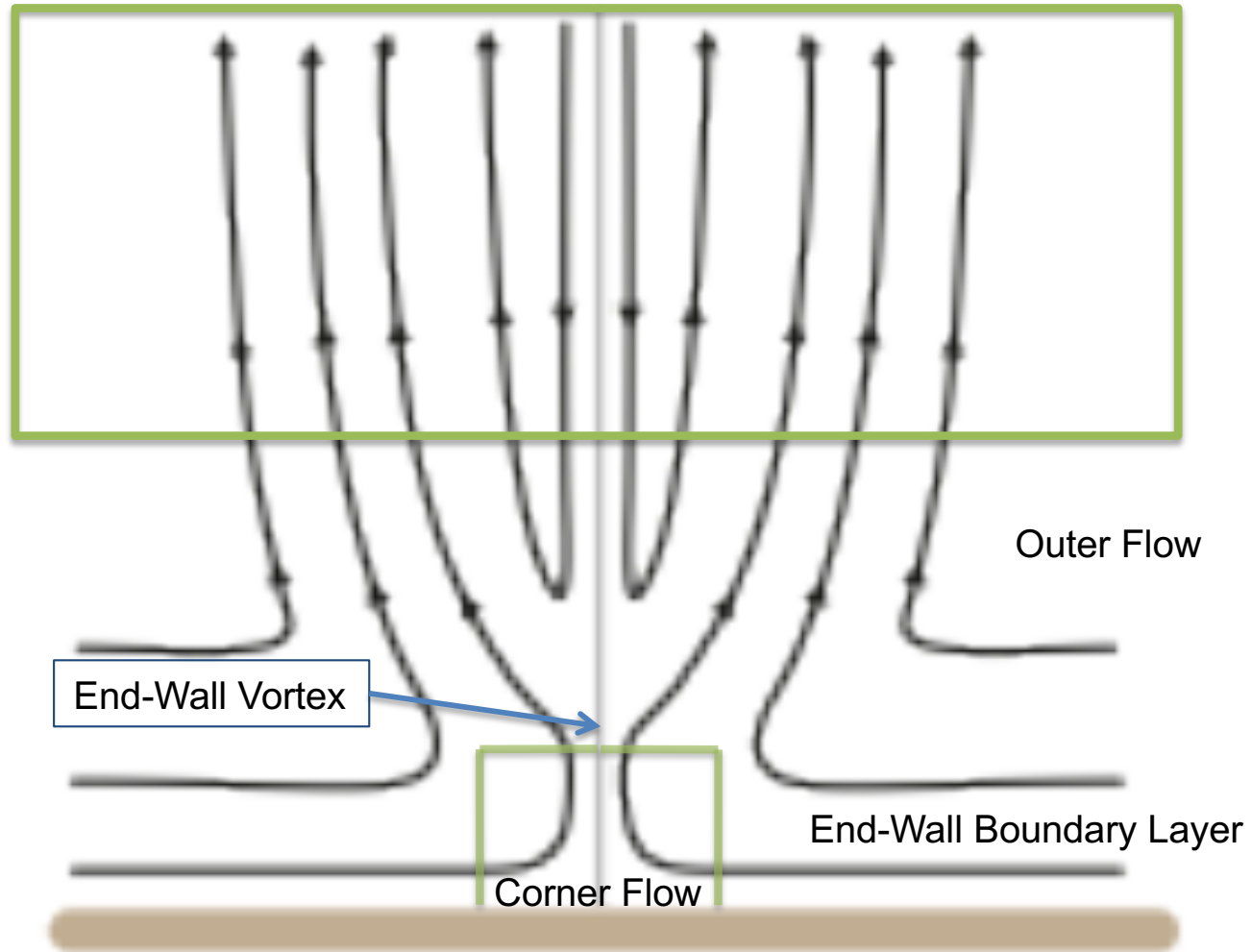


Steady Solution v. Swirl Ratio

time=150.00 rei= 1.00e-04 reit= 1.00e-03 swirl= 1.80e-01
rwid=2.0 hite=1.0 order=3 in=181 jn=181 prim



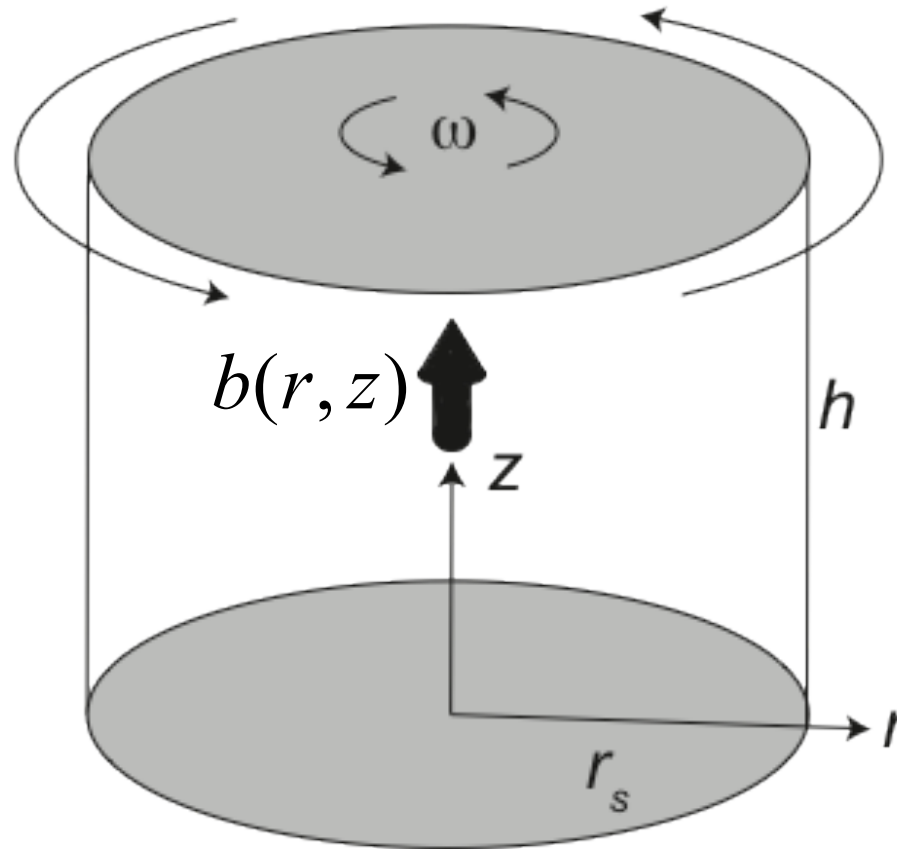
Two-Celled Vortex



The Two-Celled Vortex

Fiedler Chamber

Boundary condition
 $[u, v, w] = 0$



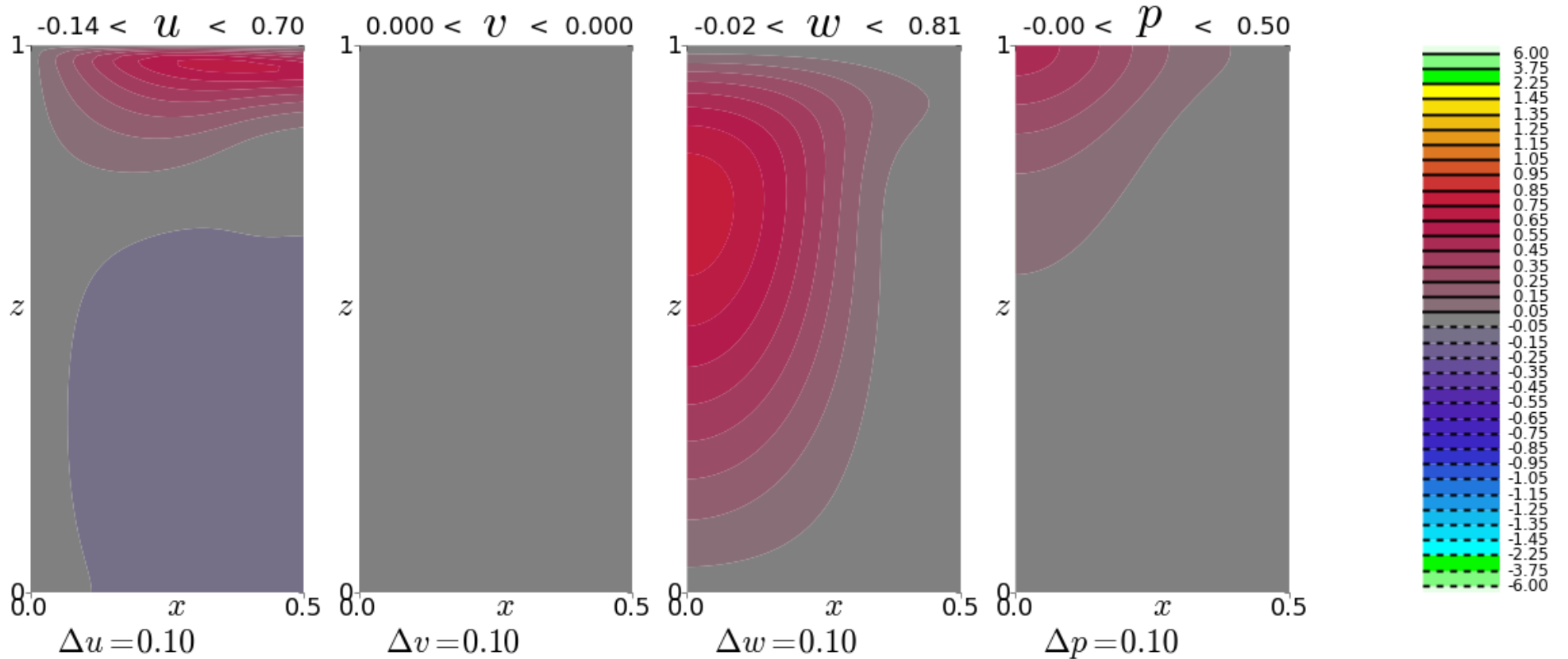
Boundary condition @ $z = 0$

Eliminate lower boundary layer
 / zero-stress condition $\rightarrow \left[\frac{\partial u}{\partial z}, \frac{\partial v}{\partial z}, w \right] = 0$

Two-Celled Vortex

Steady Solution v. Swirl Ratio

time=150.00 rei= 1.00e-04 reit= 1.00e-03 swirl= 0.00e+00
rwid=2.0 hite=1.0 order=3 in=181 jn=181 prim

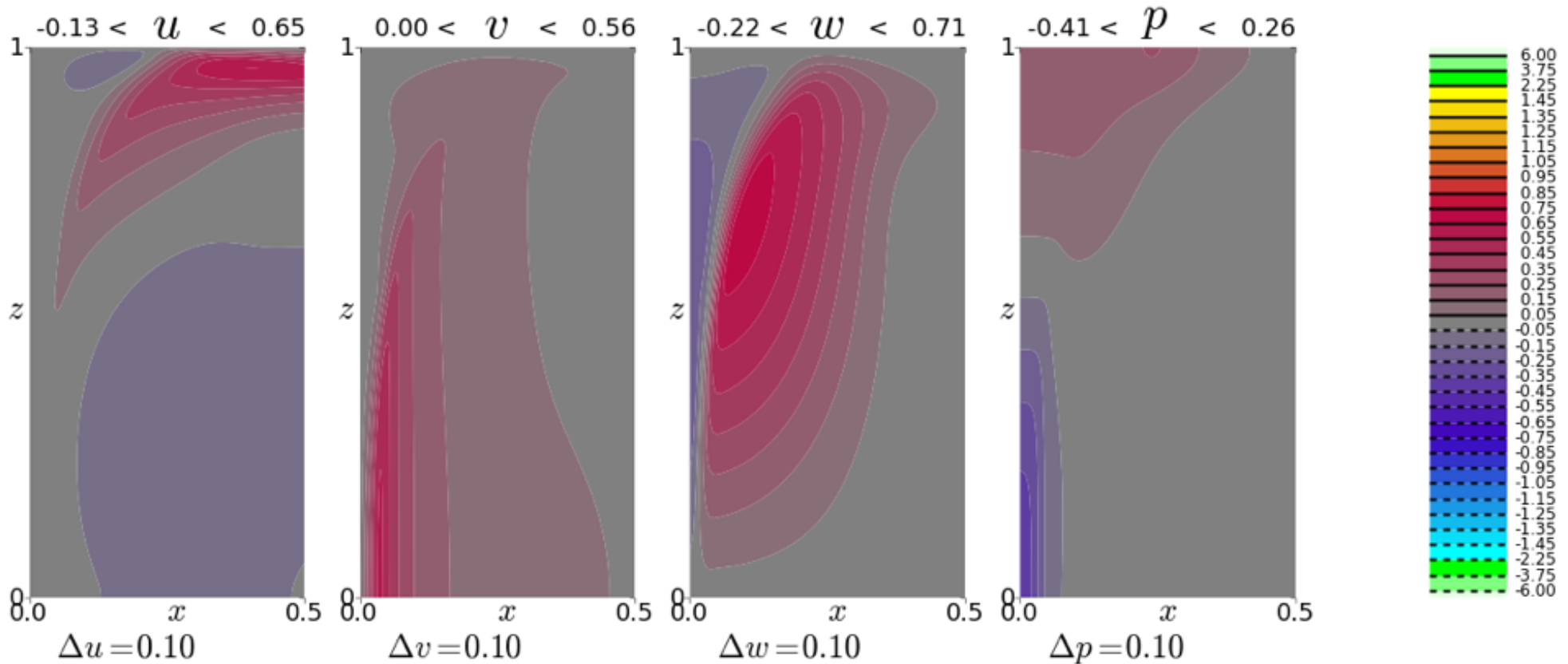


Free-Slip @ $z=0$

Two-Celled Vortex

Steady Solution v. Swirl Ratio

time=150.00 rei= 1.00e-04 reit= 1.00e-03 swirl= 2.00e-02
rwid=2.0 hite=1.0 order=3 in=181 jn=181 prim

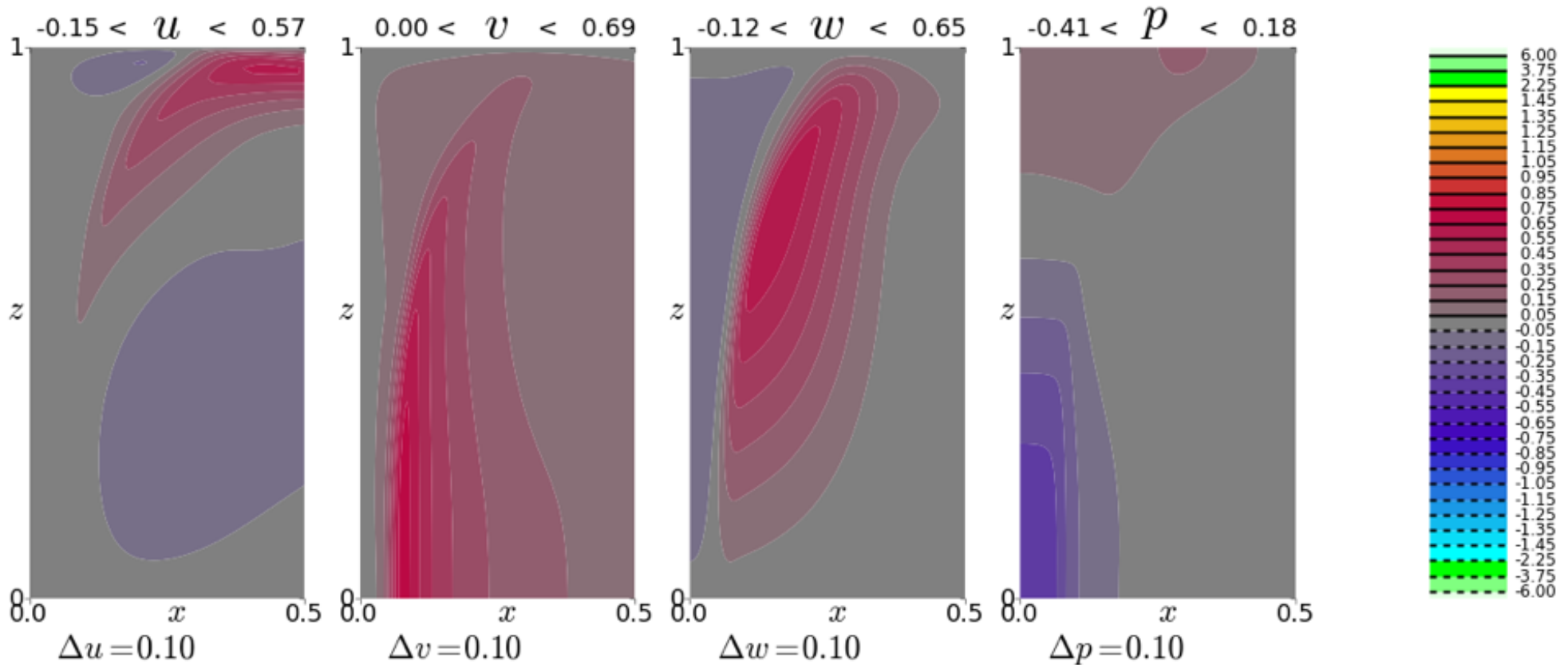


Free-Slip @ $z=0$

Two-Celled Vortex

Steady Solution v. Swirl Ratio

time=150.00 rei= 1.00e-04 reit= 1.00e-03 swirl= 5.00e-02
rwid=2.0 hite=1.0 order=3 in=181 jn=181 prim

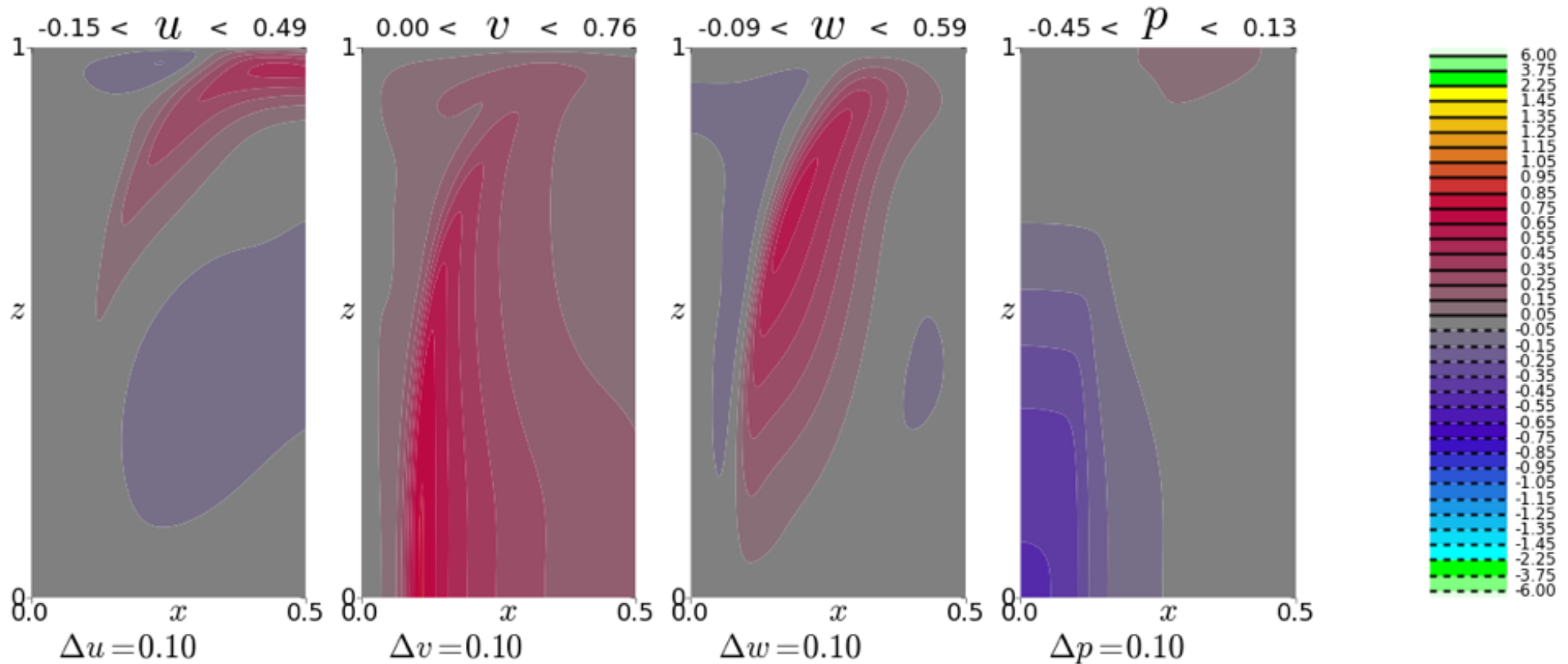


Free-Slip @ $z=0$

Two-Celled Vortex

Steady Solution v. Swirl Ratio

time=150.00 rei= 1.00e-04 reit= 1.00e-03 swirl= 1.00e-01
rwid=2.0 hite=1.0 order=3 in=181 jn=181 prim

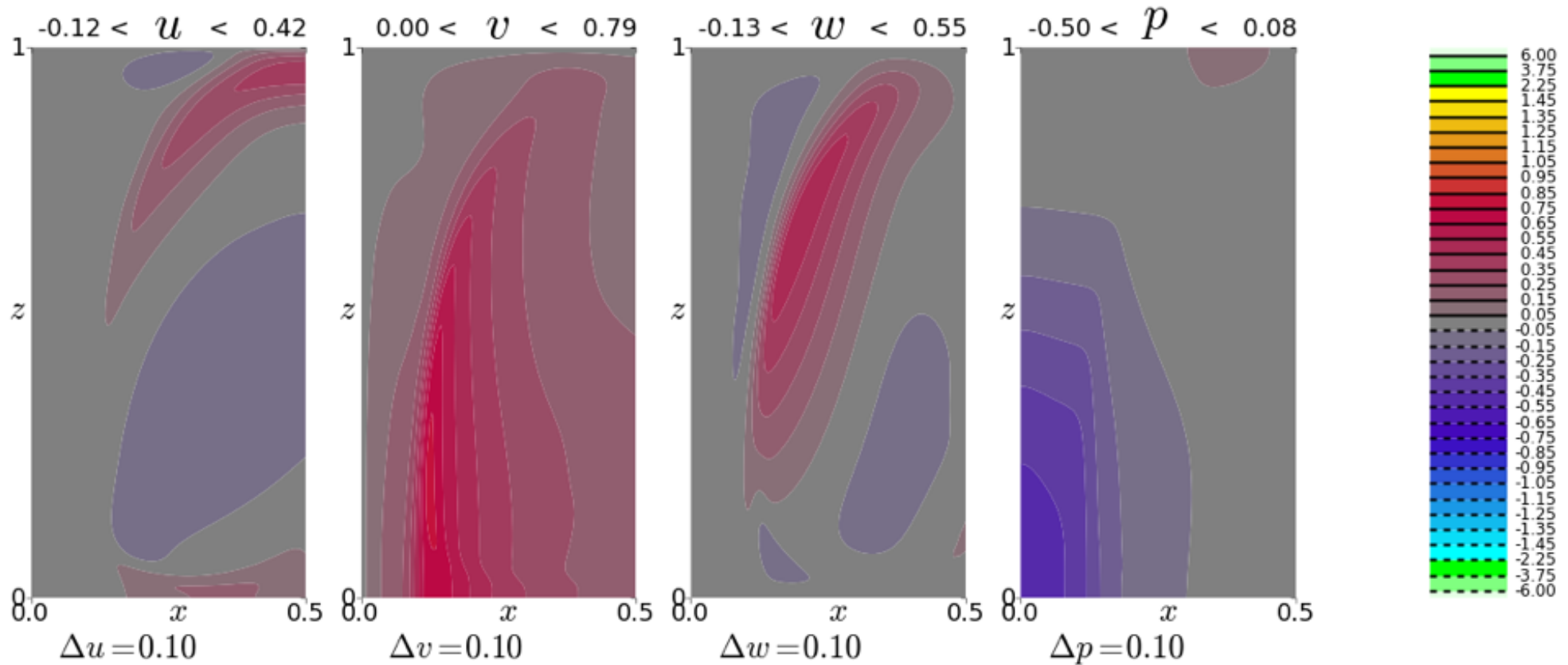


Free-Slip @ $z=0$

Two-Celled Vortex

Steady Solution v. Swirl Ratio

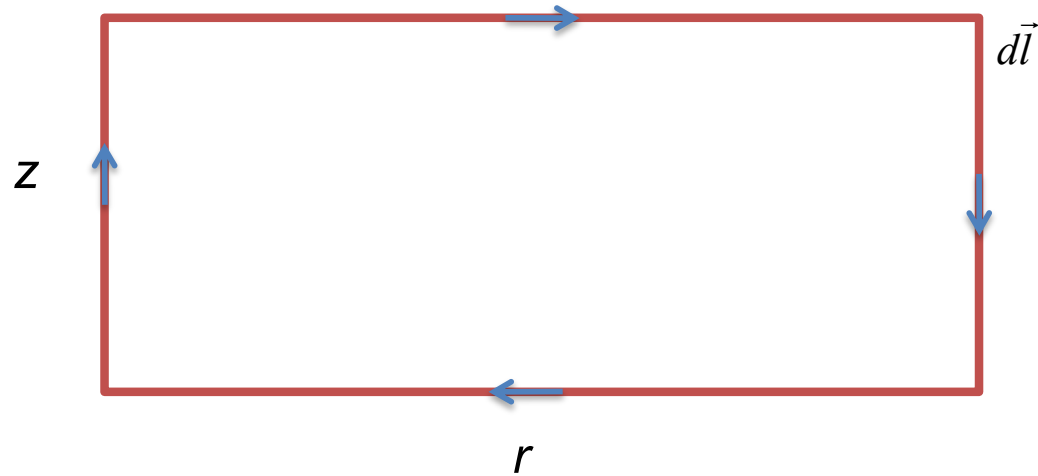
time=150.00 rei= 1.00e-04 reit= 1.00e-03 swirl= 1.80e-01
rwid=2.0 hite=1.0 order=3 in=181 jn=181 prim



Free-Slip @ $z=0$

Two-Celled Vortex

Circulation Around the Domain

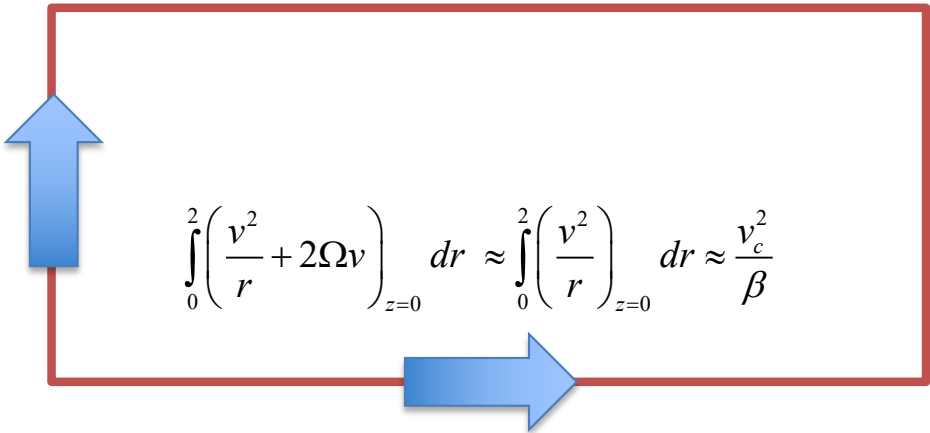


$$\frac{\partial}{\partial t} \oint \vec{u} \cdot d\vec{l} = \oint \vec{E} \cdot d\vec{l}$$

At steady state and applying boundary conditions $\rightarrow$

$$0 = \int_0^1 b|_{r=0} dz - \int_0^2 \left(\frac{v^2}{r} + 2\Omega v \right)_{z=0} dr + \oint D \cdot dl$$

Two-Celled Vortex: Balance of Buoyancy and Centrifugal Tendencies



$$\int_0^1 b|_{r=0} dz = \frac{1}{2}$$

$$\int_0^2 \left(\frac{v^2}{r} + 2\Omega v \right)_{z=0} dr \approx \int_0^2 \left(\frac{v^2}{r} \right)_{z=0} dr \approx \frac{v_c^2}{\beta}$$

$$v_c \approx \sqrt{\frac{\beta}{2}}$$

Thermodynamic Speed
 $\beta = 1$ (Rankine Vortex)

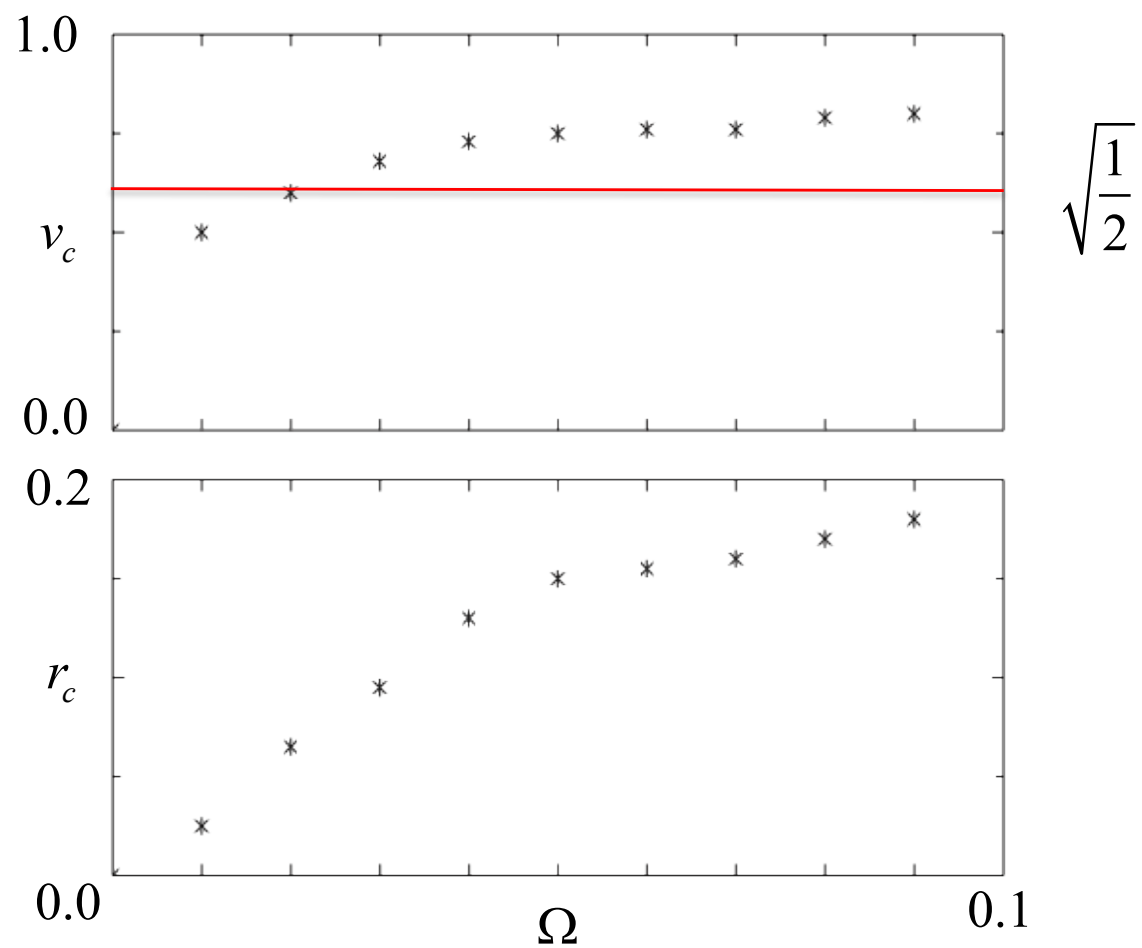
Conservation of Angular Momentum

$$r_c v_c + \Omega r_c^2 \approx r_e v_e + \Omega r_e^2$$

$$r_c \propto \Omega$$

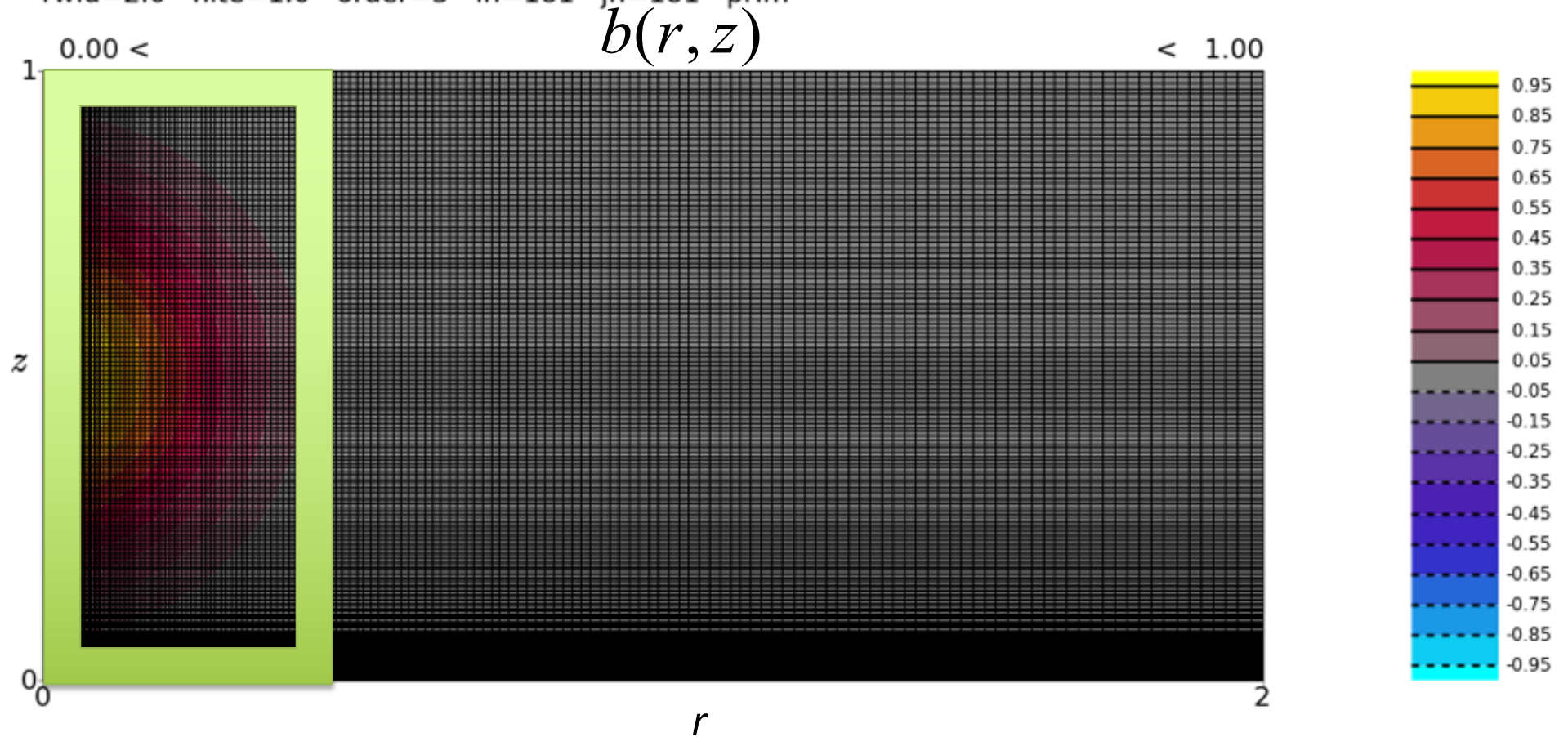
Core size Increases with Swirl Ratio

Core Size and Max Velocity from Free-Slip Two-Celled Vortex Experiments

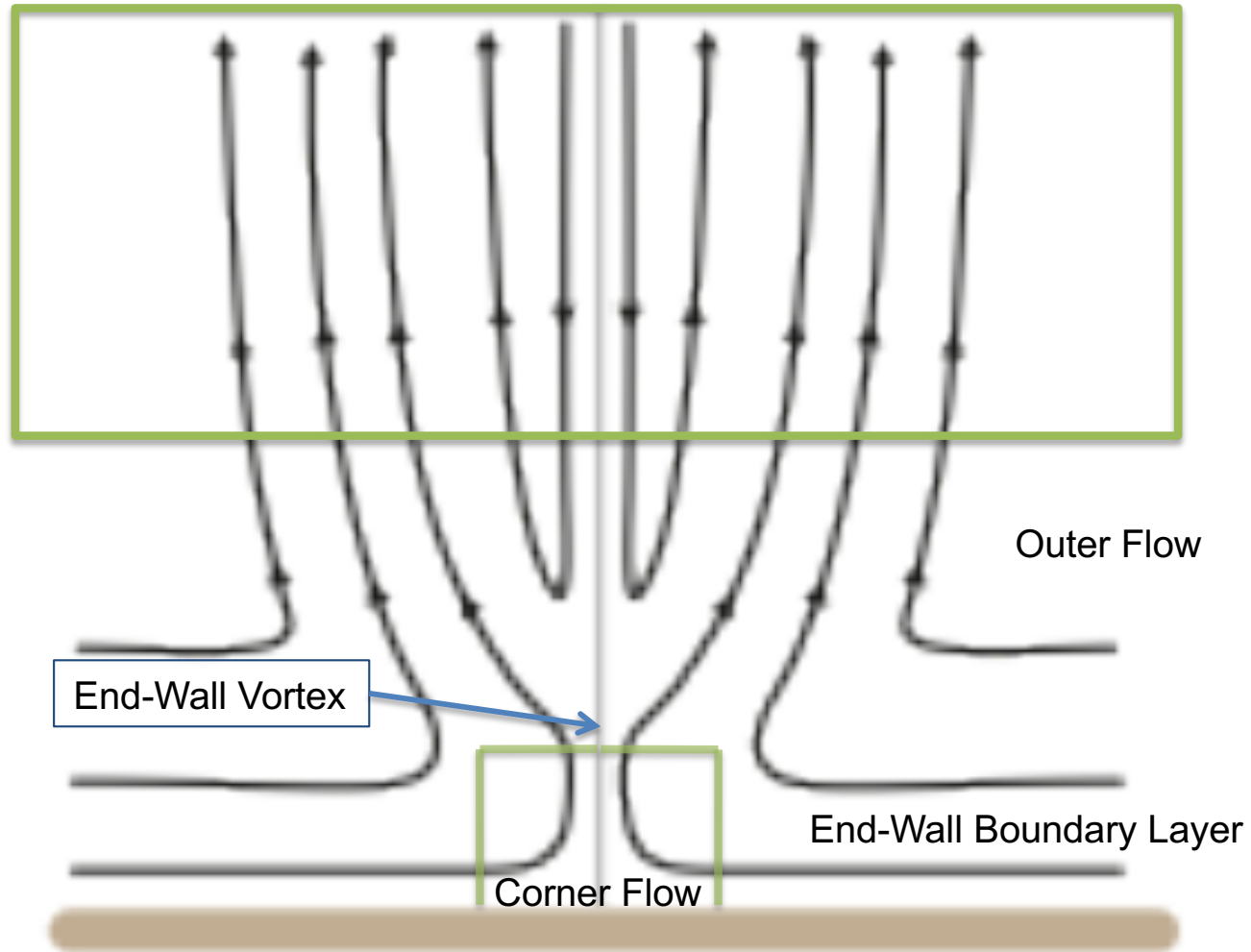


Imposed Buoyancy Force and Grid

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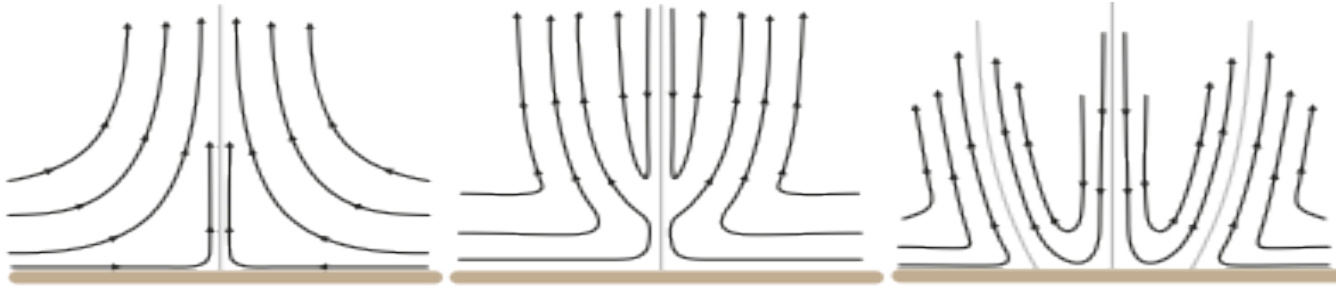


Two-Celled Vortex



Summary

1. Fiedler Chamber also produces a realistic range of vortex structures



2. Free-slip conditions eliminate the surface boundary layer and corner flow →
3. Two-celled vortex has its own distinct dynamics, essentially the classic mechanism of conservation of angular momentum

