# The E-epsilon PBL Scheme in the WRF Model

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# Outline

□An introduction to the E-epsilon scheme (EEPS)

The evaluation over the Southeast Pacific (SEP)

The evaluation over the South Great Plains (SGP)

Summary

# Why the EEPS scheme?

- The mixing length is no longer required in the E-ε scheme, which significantly reduced the number of lines of code.
- The *E*-ε scheme is the <u>first</u> scheme in the WRF model that uses ε for the closure of the TKE-equation.
- The *E*-ε scheme can better retain "<u>memory effects</u>" in length and velocity scales when surface condition changes.

## The E-epsilon (EEPS) PBL scheme (Zhang et al. 2020, MWR)

substituted by  $\mathbf{m}$  for momentum (K<sub>m</sub>)

- $\frac{\partial \theta}{\partial t} = \frac{\partial}{\partial z} \left( K_v \frac{\partial \theta}{\partial z} \right),$
- (1)  $\frac{dE}{dt} = K_m \left[ \left( \frac{\partial u}{\partial z} \right)^2 + \left( \frac{\partial v}{\partial z} \right)^2 \right] K_h P_{\text{buoy}} + C_1 \frac{\partial}{\partial z} \left( K_m \frac{\partial E}{\partial z} \right) \varepsilon,$

(2) 
$$\frac{d\varepsilon}{dt} = \max\left\langle \left\{ K_m \left[ \left( \frac{\partial u}{\partial z} \right)^2 + \left( \frac{\partial v}{\partial z} \right)^2 \right] - K_h P_{\text{buoy}} \right\} \right\}$$
$$\left\{ K_m \left[ \left( \frac{\partial u}{\partial z} \right)^2 + \left( \frac{\partial v}{\partial z} \right)^2 \right] \right\} \right\rangle C_3 \frac{\varepsilon}{E} - C_4 \frac{\varepsilon^2}{E}$$
$$+ C_5 \frac{\partial}{\partial z} \left( K_m \frac{\partial \varepsilon}{\partial z} \right),$$

(3) 
$$K_m = C_2 E^2 / \varepsilon$$
,  $(\boldsymbol{E}, \boldsymbol{\varepsilon}, \boldsymbol{K}_m, \boldsymbol{K}_h)$   
(4)  $K_h = \alpha K_m$ 

Detering and Etling (1985) Langland and Liou (1996) Duynkerke and Driedonks (1987)

 $K_v$  is the vertical mixing coefficient with the subscript v

**h** for heat and moisture  $(K_h)$ 

C1: 1.35	$E = 1 \times 10^{-4}$
C2: 0.09	$L_{min} = 1 \times 10$
C3: 1.44	$\varepsilon_{min} = 1 \times 10^{-6}$
C4: 1.92	Background K <sub>m</sub> = 0.1
C5: 0.77	K <sub>h</sub> = 0.01

A few iterations with smaller time steps are necessary for numerical stability when time step is very large

## **Prognostic Equations**

$$\alpha = \begin{cases} 1.16, -----R_i \ge 0.16, \\ 1.318 \frac{(0.2231 - R_i)}{(0.2341 - R_i)}, ----R_i < 0.16, \end{cases} \qquad R_i = P_{buoy} \left| \frac{\partial V}{\partial z} \right|^{-2}$$

$$P_{buoy} = g \frac{\partial \ln \theta_{v}}{\partial z} = g \left[ A \left( \frac{\partial \ln \theta}{\partial z} + \frac{L_{vi}}{C_{p}T} \frac{\partial q_{vis}}{\partial z} \right) - \frac{\partial q_{t}}{\partial z} \right]$$

$$P_{buoy} = g \frac{\partial \ln \theta_{v}}{\partial z} = g \left[ A \left( \frac{\partial \ln \theta}{\partial z} + \frac{L_{vi}}{C_{p}T} \frac{\partial q_{vis}}{\partial z} \right) - \frac{\partial q_{t}}{\partial z} \right]$$

$$P_{outhorson and Emanuel (1987)}$$

$$P_{vis} = (1 - W_{l})q_{sw} + W_{l}q_{si}$$

$$L_{vi} = (1 - W_{l})L_{v} + W_{l}L_{s}$$

$$W_{l} = MAX \left[ 0.0, MIN(1.0, \frac{T_{0} - T}{T_{0} - 233.16}) \right]$$

q<sub>t</sub>: the sum of the mixing ratios of cloud water, rain water, cloud ice, snow and graupel q<sub>vis</sub>: the saturation mixing ratio of water vapor

- L<sub>vi</sub>: the latent heat of phase change
- L<sub>v</sub>: the latent heat of condensation
- L<sub>s</sub>: the latent heat of sublimation

## **Prognostic Equations**

The lower boundary conditions at the lowest model level:

$$E_{s} = \begin{cases} 3.75u_{*}^{2}, -----R_{is} > 0.0, \\ 3.75u_{*}^{2} + 0.2w_{*}^{2} + (-z_{km}/L)^{2/3}u_{*}^{2}, ----R_{is} \le 0.0, \end{cases}$$

$$R_{is} = \frac{gz_{km} \ln(\theta_{vkm} / \theta_{vs})}{|V_{km}|^{2}}$$

$$\varepsilon_{s} = \frac{u_{*}^{3}}{kz_{km}}$$

km is the lowest model level
u∗ is the friction velocity
L is the Monin-Obukhov length
k is the von Kármán constant 0.4

The upper boundary conditions at the model top are E=0 and  $\epsilon$ =0

## **Prognostic Equations**

A nonlocal term is included in vertical eddy mixing of heat and moisture

$$\frac{\partial \theta}{\partial t} = \frac{\partial}{\partial z} K_h (\frac{\partial \theta}{\partial z} - \gamma_t), - - \gamma_t = \frac{5H_s}{w_* h}$$
$$\frac{\partial q}{\partial t} = \frac{\partial}{\partial z} K_h (\frac{\partial q}{\partial z} - \gamma_q), - - \gamma_q = \frac{5H_q}{w_* h}$$
$$H_s = HFX(\rho C_p)^{-1}$$
$$H_q = QFX(\rho)^{-1}$$

h is the boundary layer height, which is defined as the lowest level the modified Bulk Richardson Number exceeds a critical value of 0.25 w\* is the convective velocity

# The TKE dissipative heating

$$\frac{\partial T}{\partial t} = \frac{\varepsilon}{c_p}$$

#### The evaluation over the Southeast Pacific (SEP)





TKE and EDR are meridionally averaged between 18° and 22°N





Meridionally averaged between  $18^\circ$  and  $22^\circ N$ 

#### Shading: cloud mixing ratio

Contour: virtual potential temperature

### The PBL height diagnosed by each scheme



The planetary boundary layer height (PBL height; unit: m) diagnosed by each PBL scheme.







#### The evaluation over the South Great Plains (SGP)



Verification data are from The LAFE 2017 Compared the EEPS with The YSU, MYNN and UW

3 km grid spacing51 vertical levels21 levels below 2.5 km

Five consecutive days 12 UTC 27 Aug – 12 UTC 1 Sep Five runs (36-hr) for each scheme

IC&BC: GFS Soil data: 3-month spin-up



#### TKE (EDR) on time-height space

0.06

0.1











# Summary

- The EEPS and YSU schemes perform comparably over both regions, while the MYNN scheme performs differently in many aspects, especially over the SEP.
- Compared with observations, the UW scheme produces the best PBL height over the SEP. The MYNN produces too high PBL height over the western part of the SEP while both the YSU and EEPS schemes produce too low PBL and cloud-top heights.
- The differences among the PBL schemes in simulating the PBL features over the SGP are relatively small.