



A New Combined Local and Non-Local Boundary Layer Model: ACM2

Jonathan Pleim
NOAA/ARL
USEPA/ORD
RTP, NC

Outline

- Model development
- 1-D testing and evaluation
 - Large Eddy Simulation (LES)
 - GABLS Experiment (CASES99)
- MM5 testing and evaluation
- WRF implementation will soon be ready



Purpose

- Develop a simple PBL model that:
 - Produces realistic profiles in CBL
 - Accurate PBL heights
 - Appropriate for all stability conditions w/ minimal discontinuities
 - For both meteorology and chemistry models
 - Computationally efficient

Background

- Local flux-gradient proportionality (i.e. Eddy diffusion) is not appropriate for Convective Boundary Layers
 1. Upward heat flux penetrates to ~80% of h while potential temperature gradients are very small through most of the PBL
 2. Eddies in CBL are larger than vertical grid spacing (violates subgrid-scale assumption)
- Two common alternative approaches:

1. Gradient adjustment term:

$$\frac{\partial \theta}{\partial t} = \frac{\partial}{\partial z} \left(K_h \left(\frac{\partial \theta}{\partial z} - \gamma_h \right) \right)$$

Deardorff 1966, Troen and Mahrt 1986,
Holstlag and Boville 1993, Noh et al. 2003

2. Transient or non-local closure:

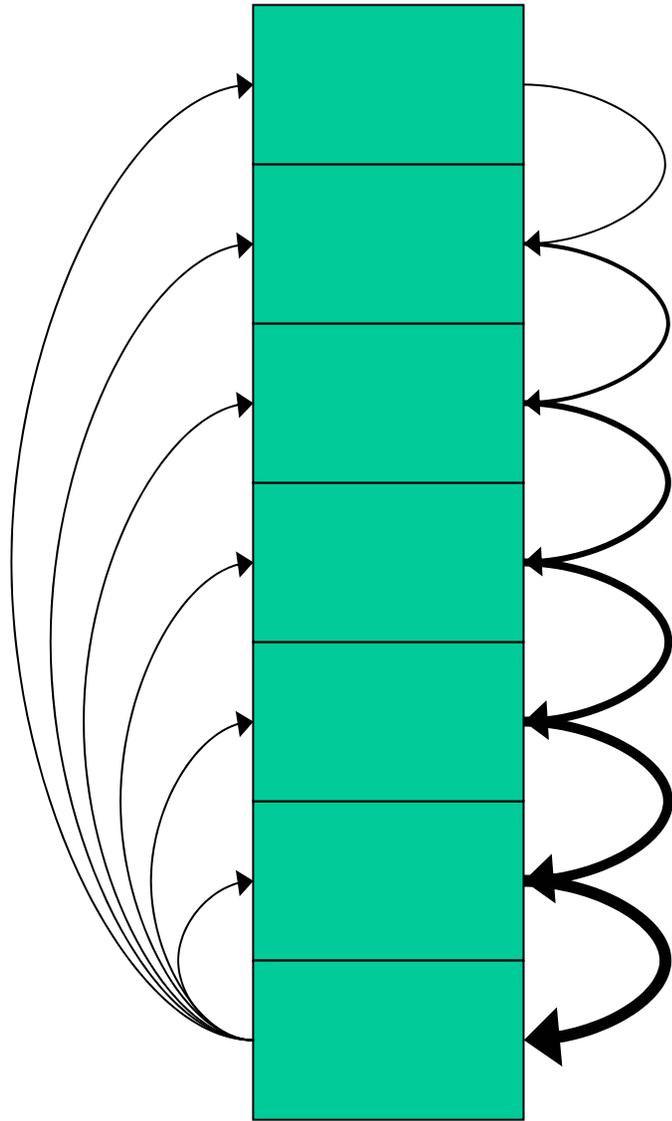
$$\frac{\partial \theta_i}{\partial t} = M_{ij} \theta_j$$

Stull 1984, Blackadar 1976,
Pleim and Chang 1992

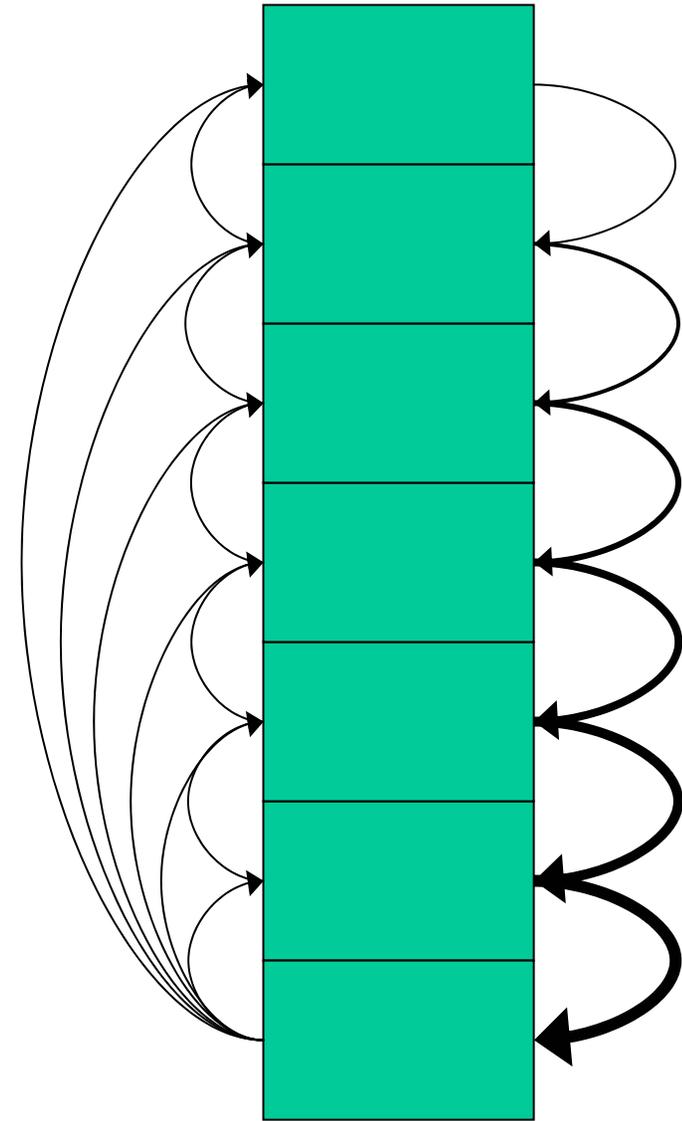
Asymmetric Convective Model (ACM)

- Original ACM
 - Simple Transient model
 - Rapid upward transport by convectively buoyant plumes
 - Gradual downward transport by compensatory subsidence
 - Part of the PX-LSM in MM5
- ACM2
 - Added eddy diffusion to ACM
 - Allows local mixing at all levels
 - More realistic (continuous) profiles in lower layers
 - Smooth transition from stable to unstable





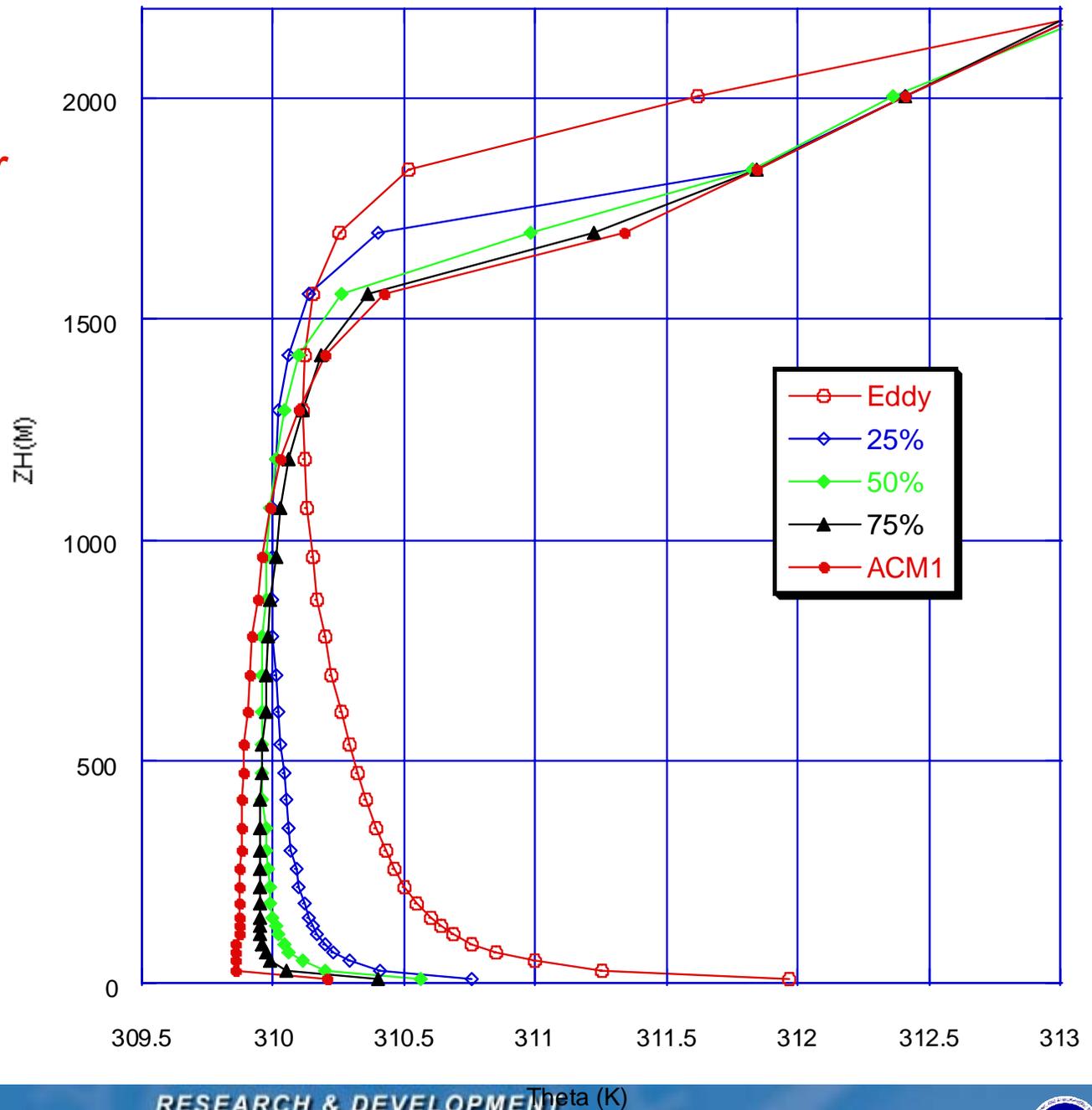
ACM



ACM2

Need to define a partitioning factor (f_{conv})

1-D experiments –
Variations in partitioning of local and non-local transport

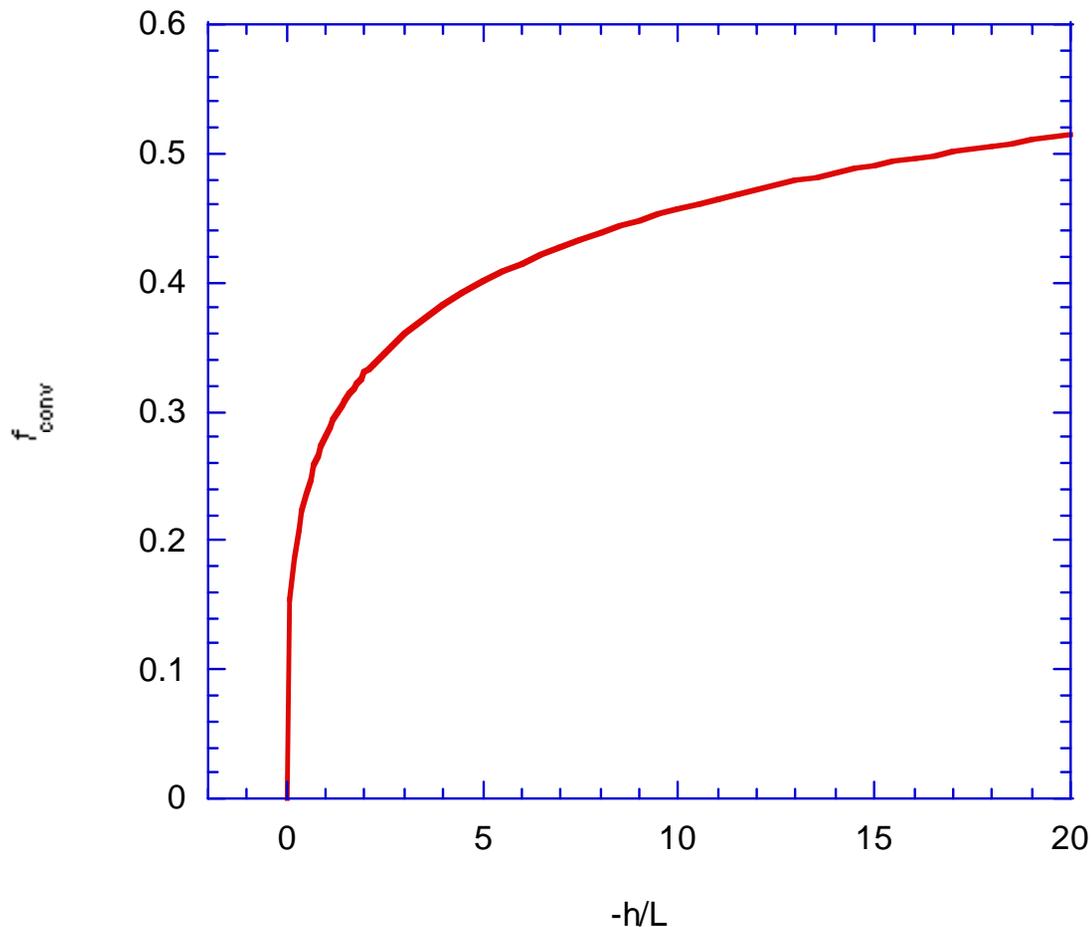


Non-local partitioning

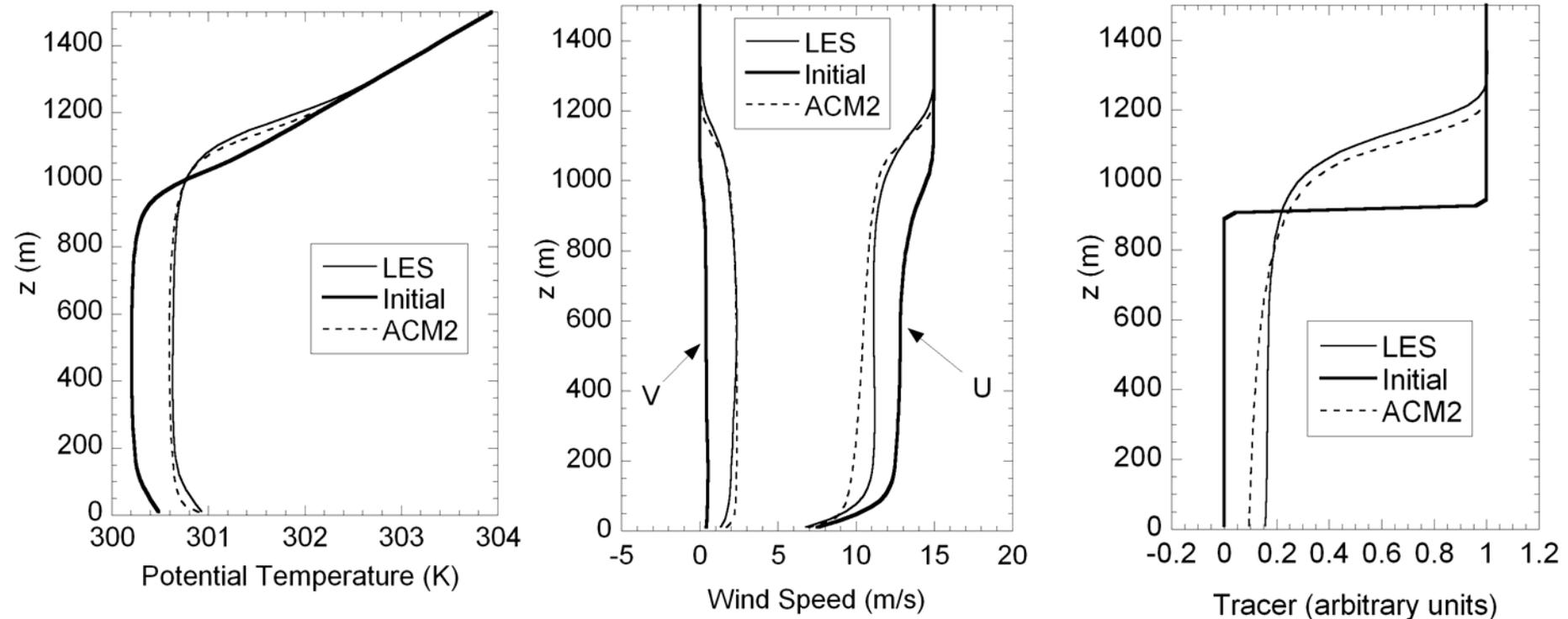
- These tests suggest that the upper limit of f_{conv} should be about 50%
- An expression for f_{conv} can be derived from gradient adjustment models (e.g. Holstlag and Boville 1993) at top of surface layer:

$$f_{conv} = \left(1 + \frac{k^{-2/3}}{0.1a} \left(-\frac{h}{L} \right)^{-1/3} \right)^{-1}$$

Non-local fraction (f_{conv}) as function of stability



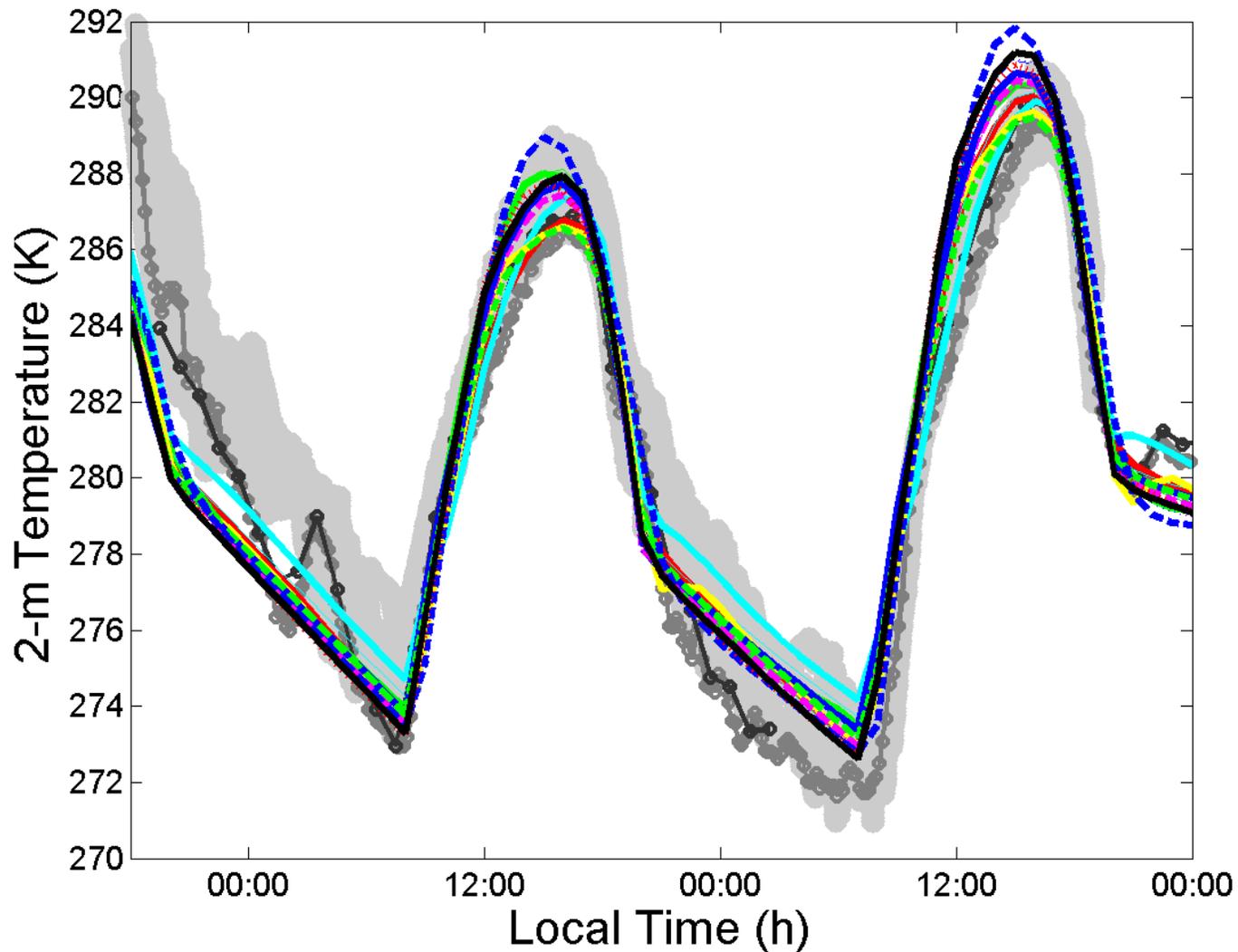
LES experiment low heat flux ($Q^* = 0.05 \text{ K m s}^{-1}$), weak cap



The second GABLS model intercomparison

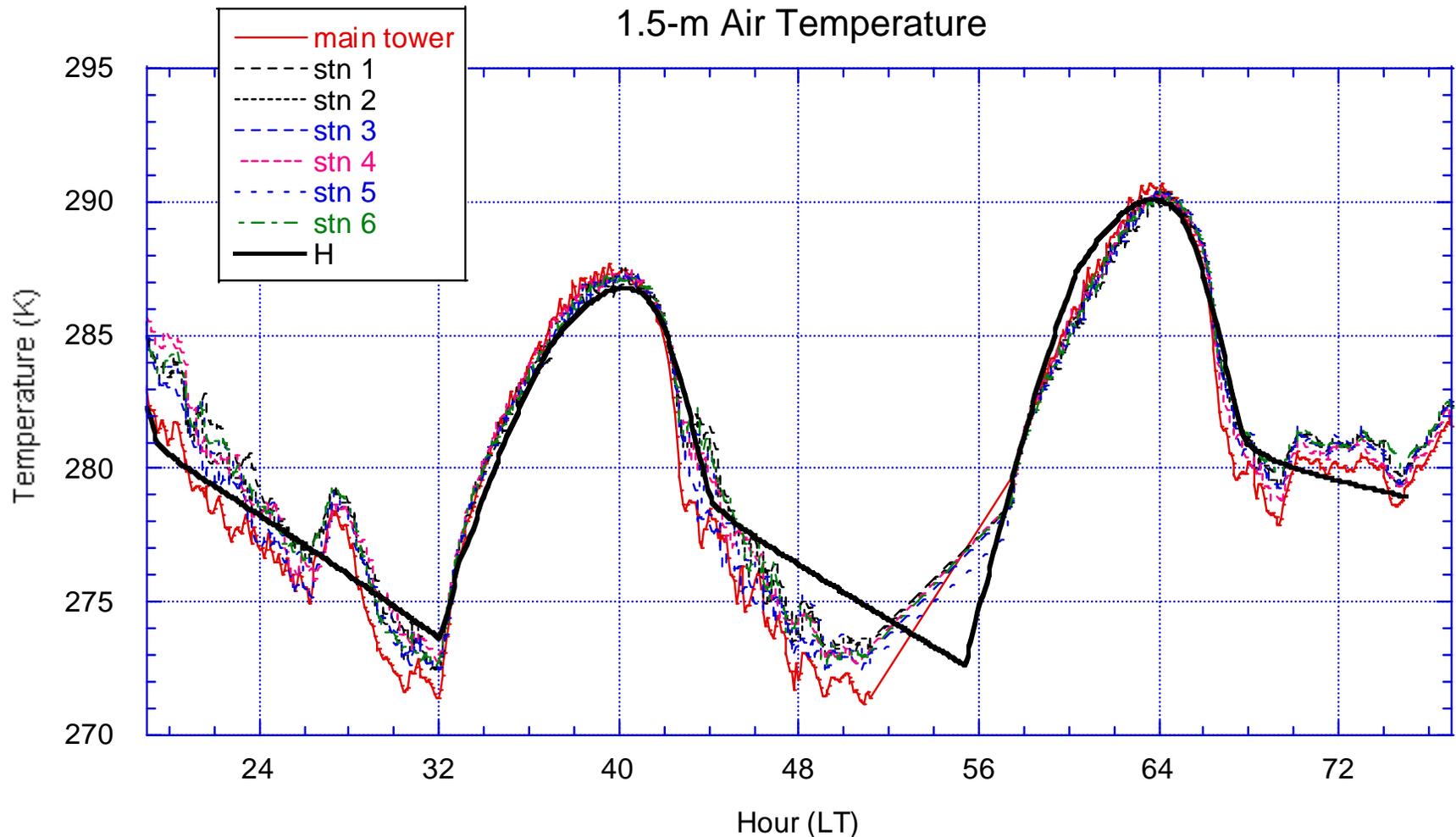
- Multi-day Intercomparison of 23 PBL models for CASES99 field study
 - Given initial profiles
 - T_g time series
 - Constant geostrophic wind
 - Large scale subsidence
 - 2.5% of potential evaporation
 - P, z_0, z_T

GABLS T-2m Intercomparison



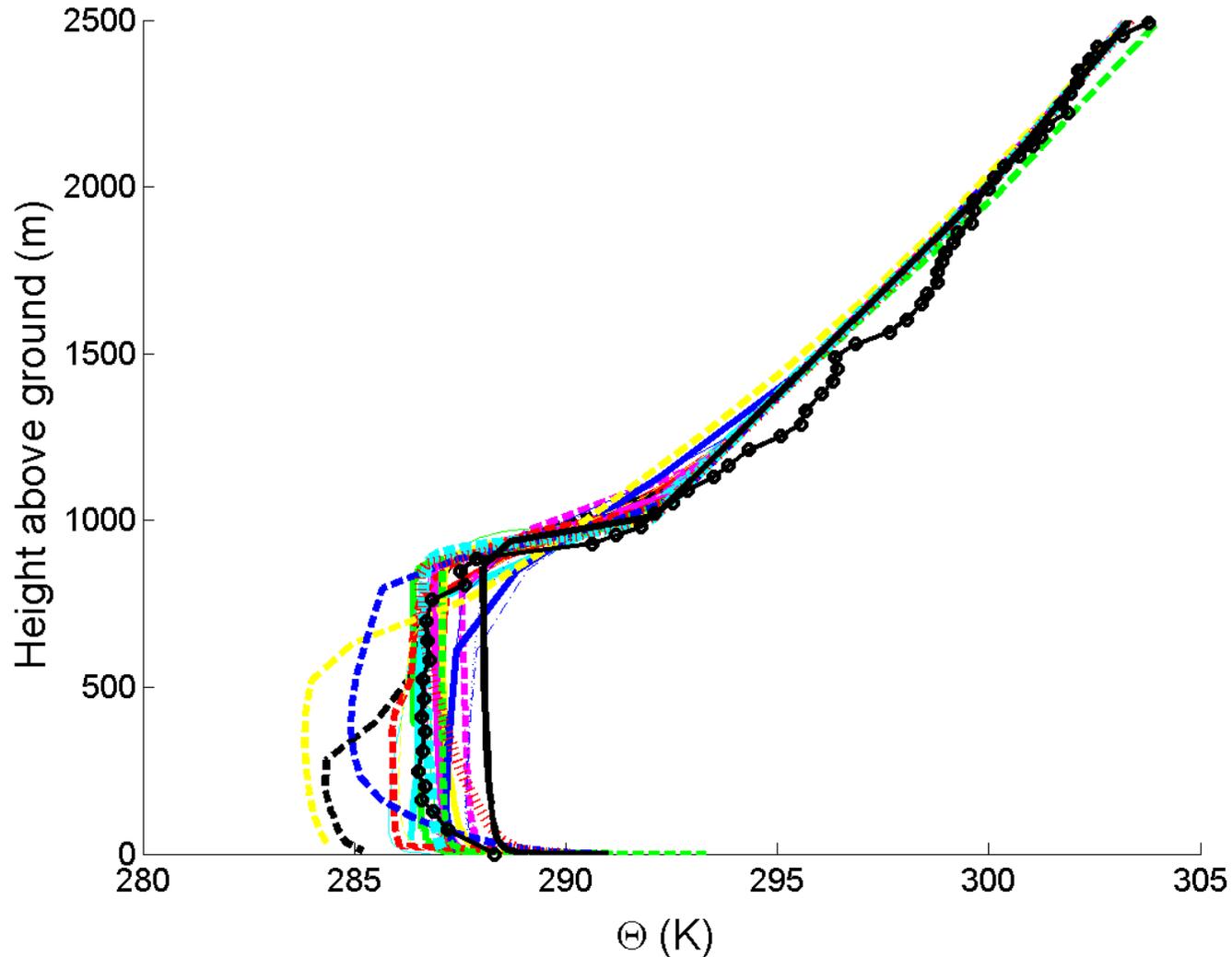
GABLS Experiment – Simulation of CASES99

October 22-24, 1999



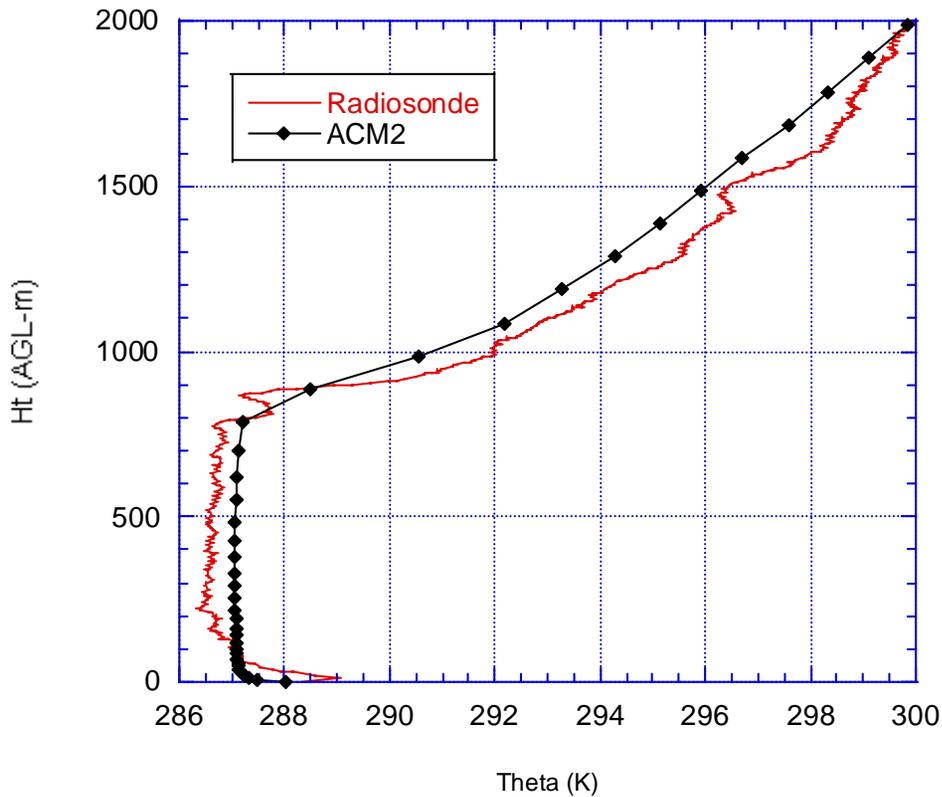
GABLS Profile intercomparison

14 LT October 23

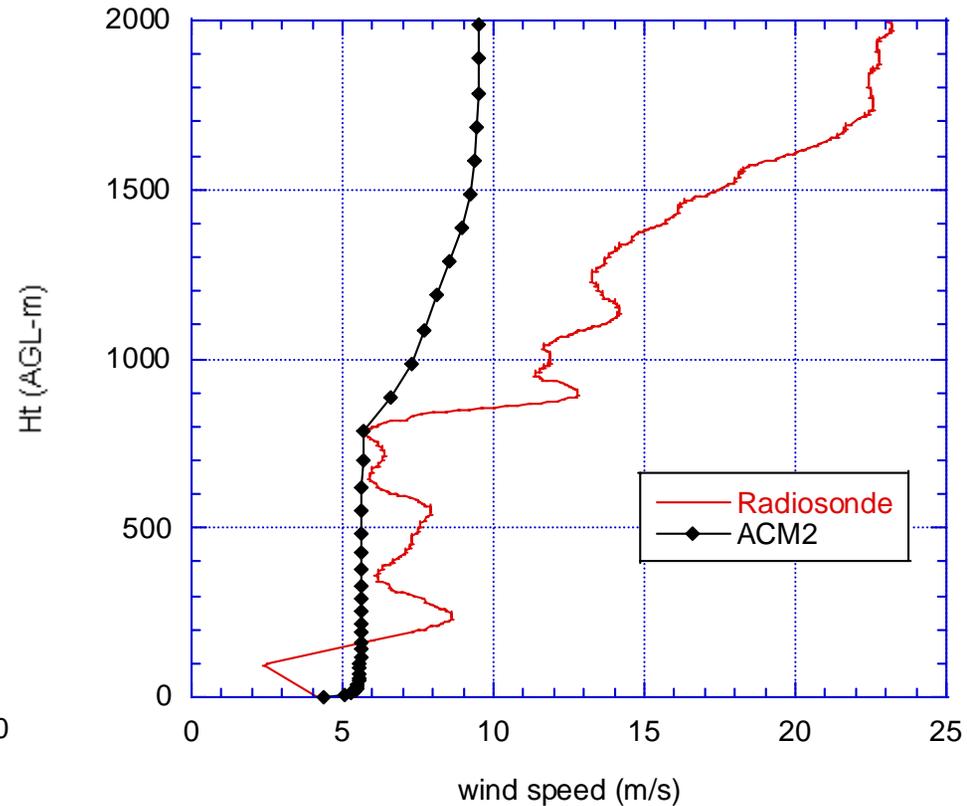


CASES99 profiles

Leon, KS October 23, 1999 - 19z



Leon, KS October 23, 1999 - 19z

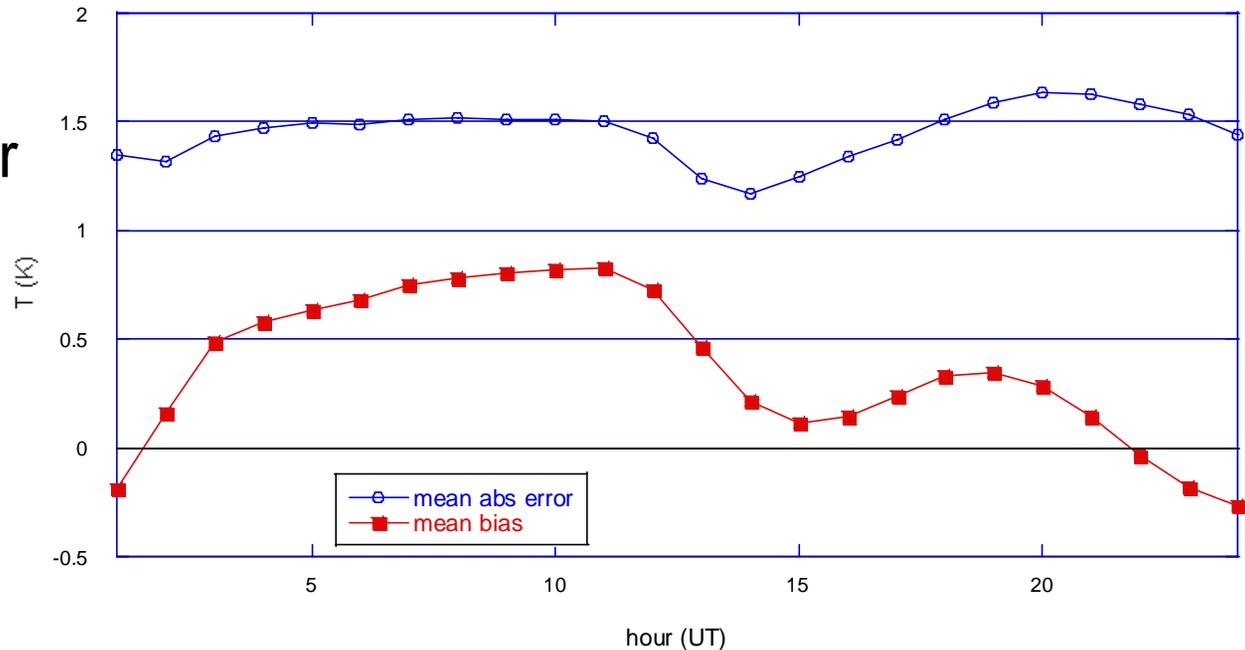
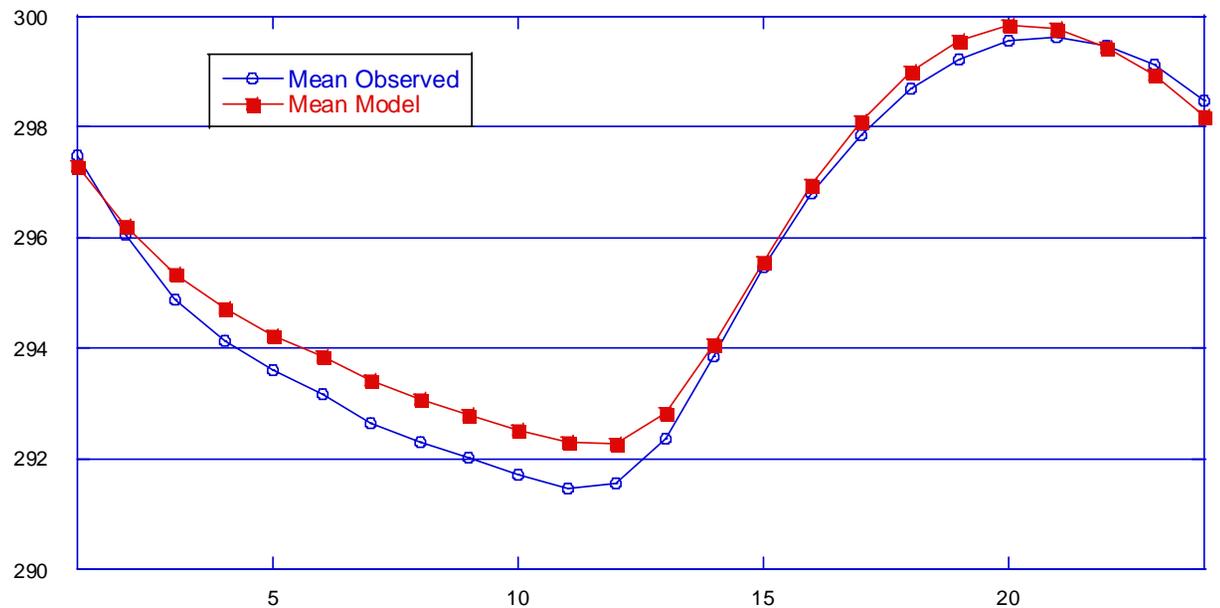


MM5 Evaluations

- Domain: 202 x 208 x 34 @ 12 km res
- Physics:
 - ACM2
 - PX LSM
 - KF2
 - Reisner 2
 - RRTM w/ Dudhia SW
- Data Assimilation:
 - Winds at all levels, T and q_v above PBL
 - Indirect soil moisture nudging
- July 13 – August 18, 2004



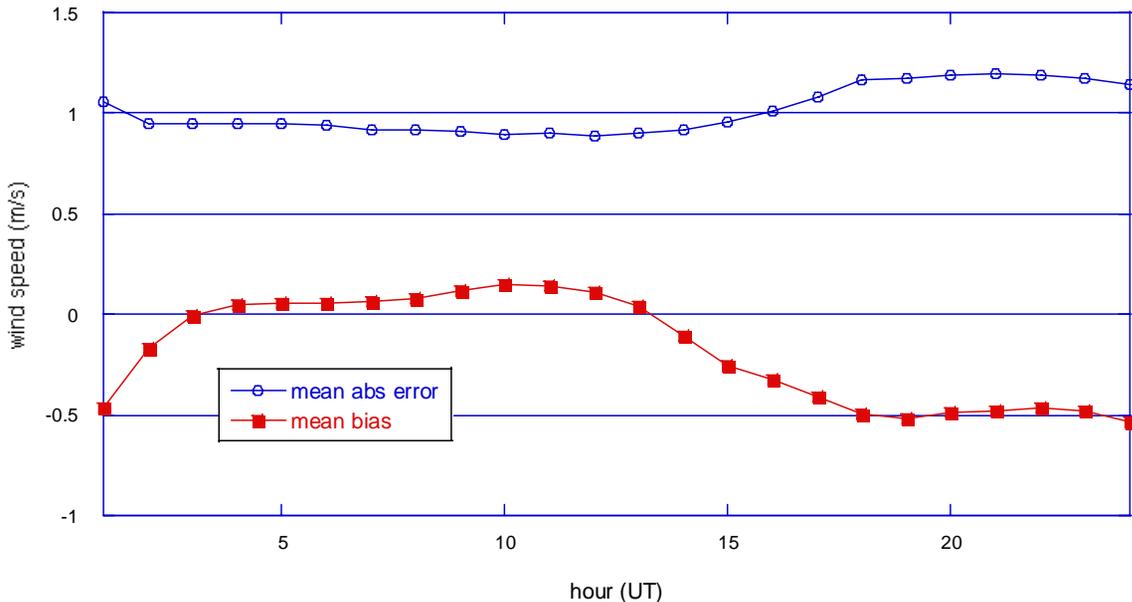
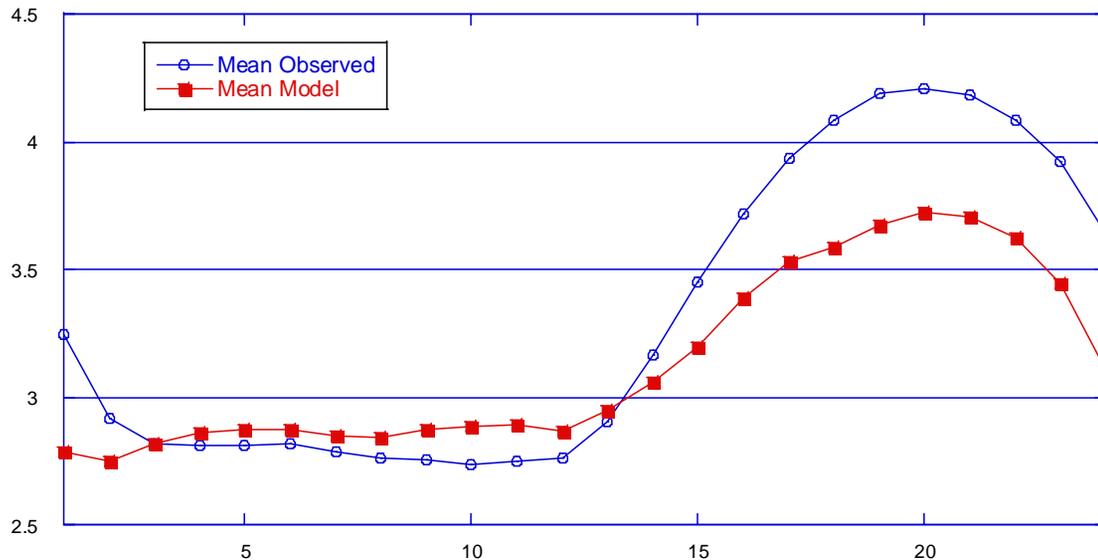
2 m Temperature Averaged over all NWS/FAA sites 7/15 – 8/18 2004



Mean Absolute Error
Mean Bias



10 m Wind speed Averaged over all NWS/FAA sites 7/15 – 8/18 2004

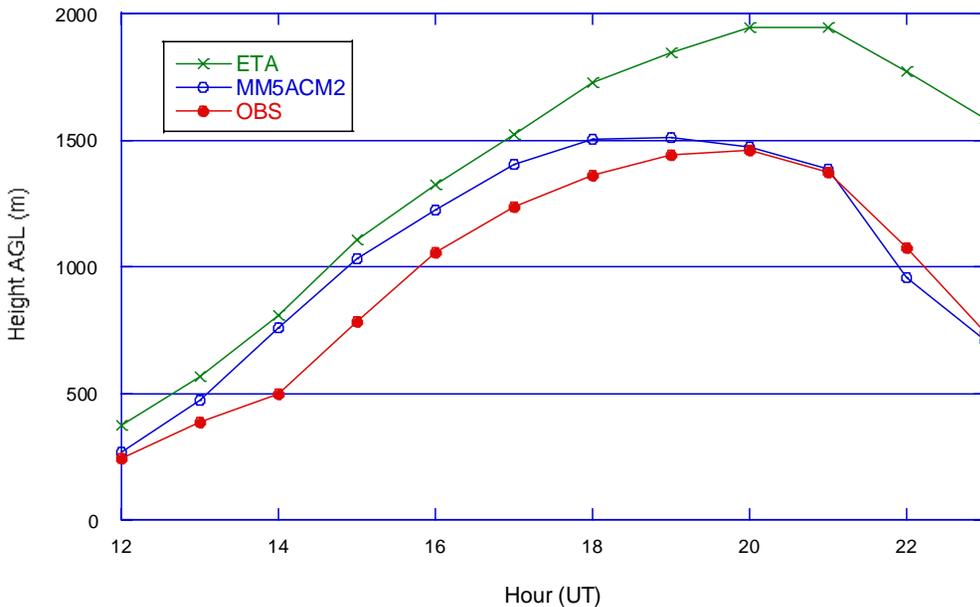
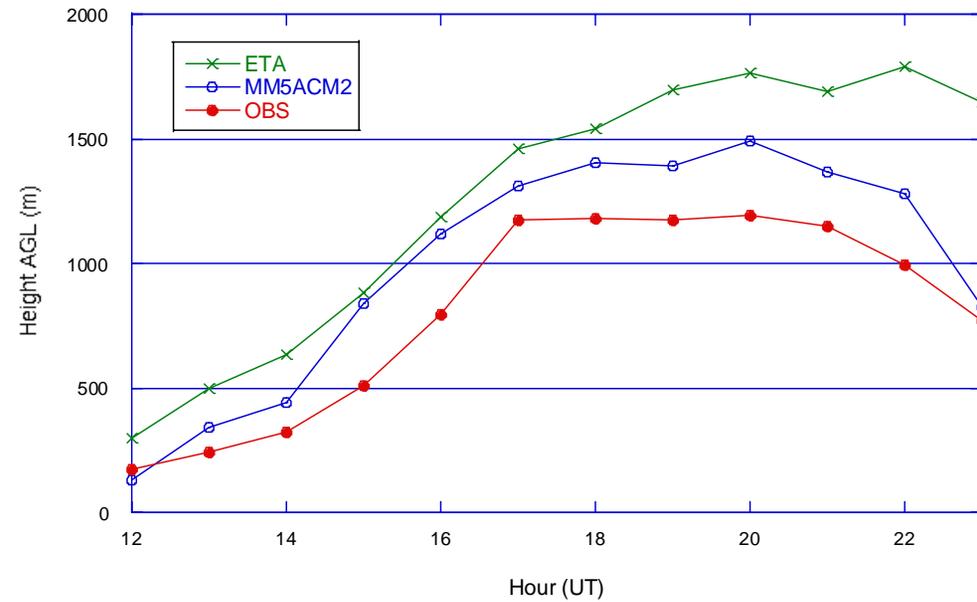


Mean Absolute Error
Mean Bias



PBL Height from Radar wind Profilers (from Jim Wilczak)

Pittsburgh, PA



Concord, NH



RESEARCH & DEVELOPMENT

Building a scientific foundation for sound environmental decisions



Conclusions

- ACM2 is a combination of local and non-local closure techniques
 - Similar capabilities to eddy diffusion w/ counter-gradient adjustment but more readily applicable to any quantity (e.g chemistry)
 - ACM2 produces more realistic near-ground profiles than ACM1
- LES and 1-D tests show accurate simulation of vertical profiles and PBL heights
- MM5 tests show good ground level performance and accurate PBL heights



Non-local Mixing rates

Convective mixing rate derived by conservation of buoyancy flux:

$$\bar{M} = B_{1+1/2} / \left[(h - z_{1+1/2}) (\theta_{v1} - \theta_{v2}) \right]$$

Buoyancy flux at top of first layer defined by eddy diffusion:

$$B_{1+1/2} = K_z(z_{1+1/2}) \frac{(\theta_{v2} - \theta_{v1})}{\Delta z_{1+1/2}}$$

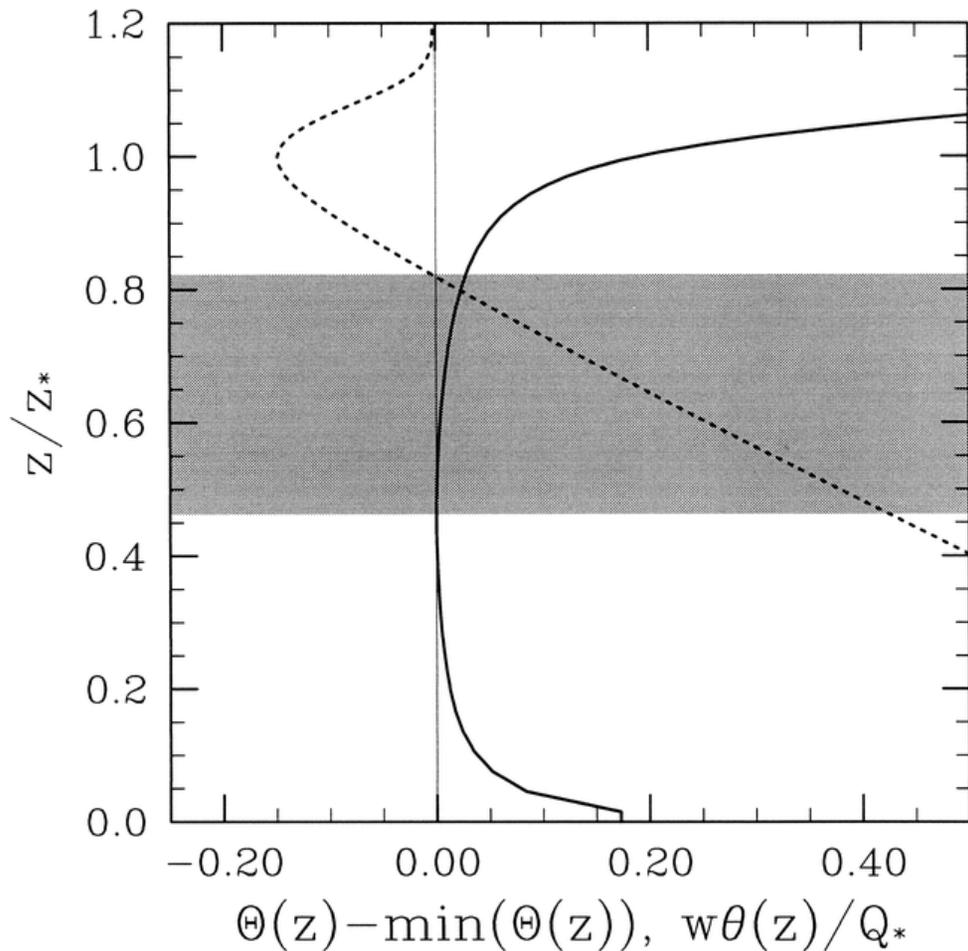
Where:

$$K_z = k \frac{u_*}{\phi\left(\frac{z_s}{L}\right)} z (1 - z/h)^2; z_s = \min(z, 0.1h)$$

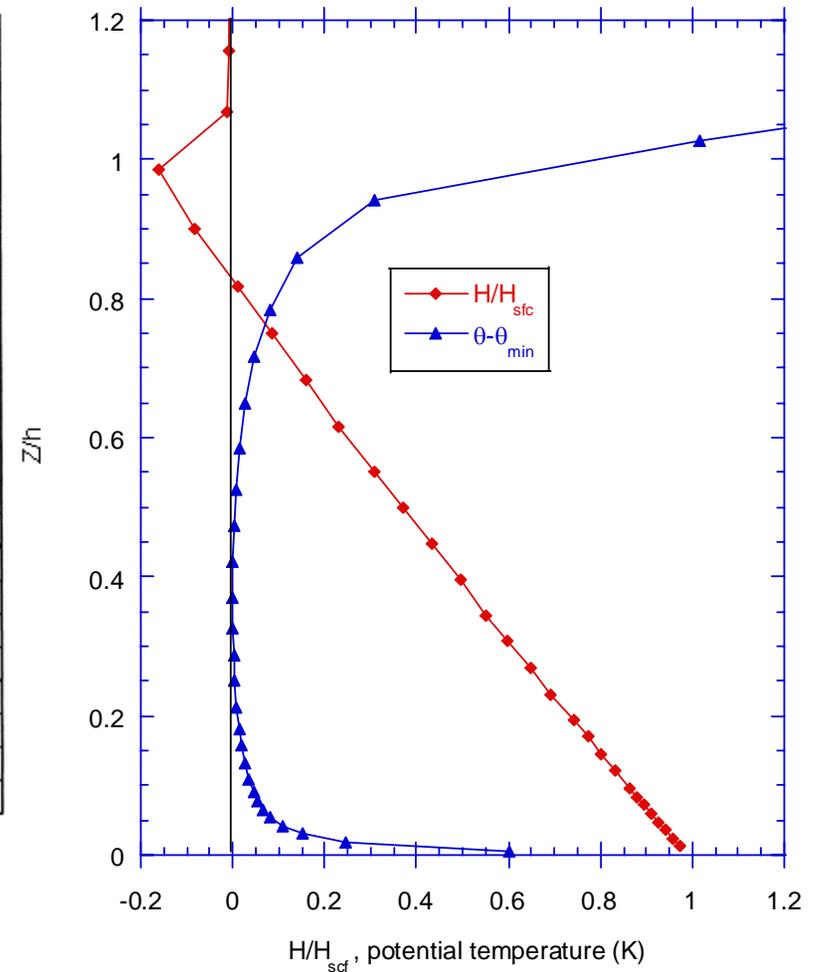
Thus, Convective mixing rate is a function of K_z but not a function of potential temperature gradient:

$$\bar{M} = \frac{K_z(z_{1+1/2})}{\Delta z_1 (h - z_{1+1/2})}$$

Normalized heat flux and potential temperature profiles

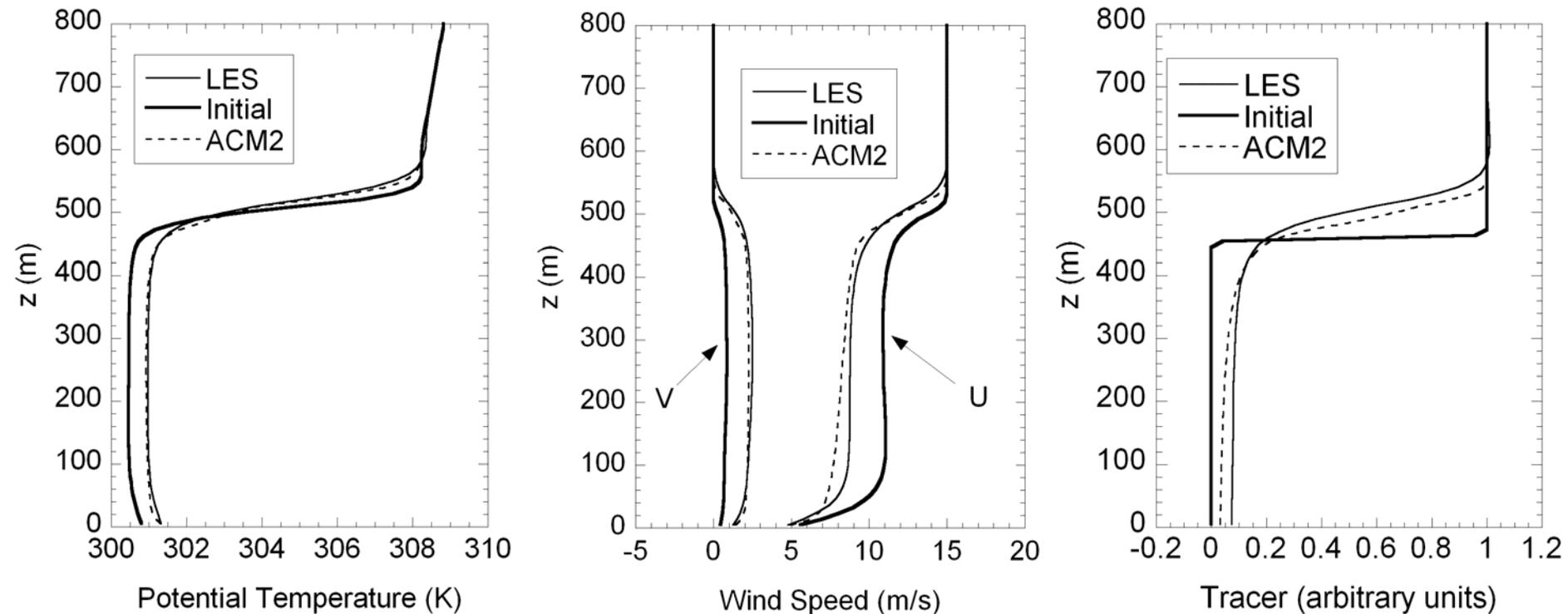


LES (Stevens 2000)

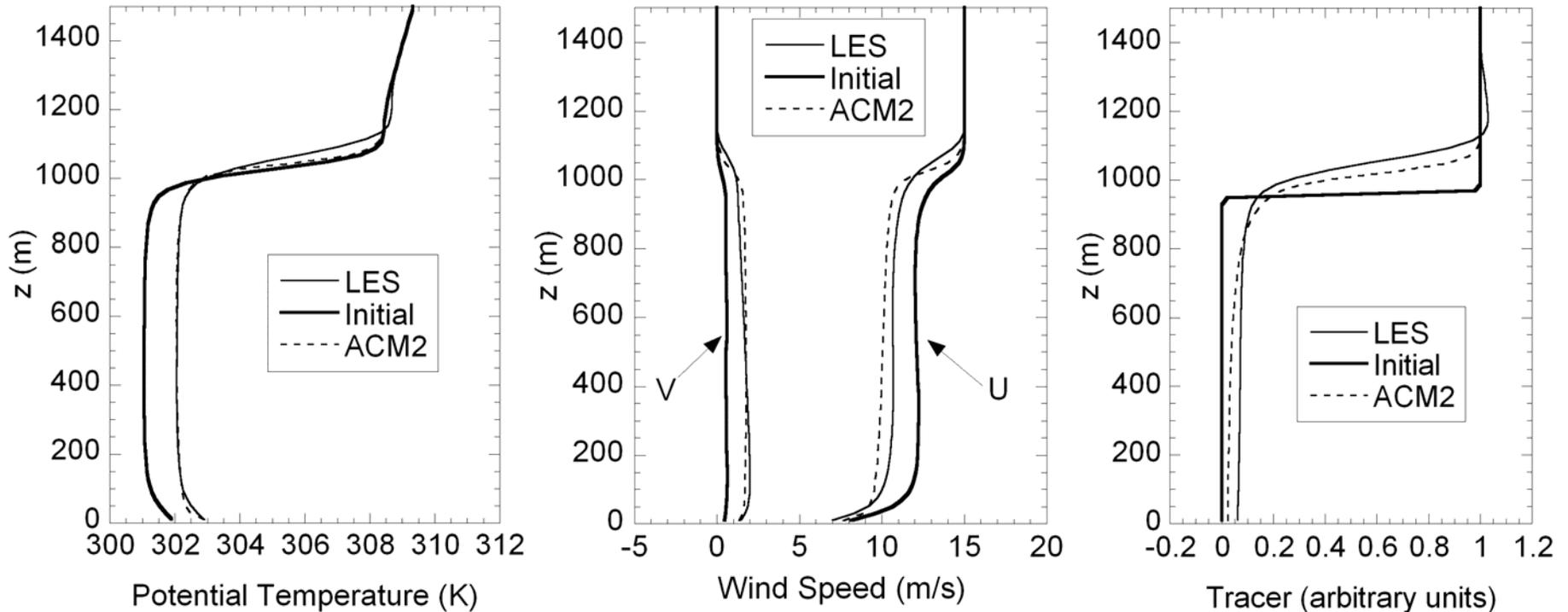


ACM2

LES experiment low heat flux ($Q^* = 0.05 \text{ K m s}^{-1}$), strong cap



LES experiment high heat flux ($Q^* = 0.24 \text{ K m s}^{-1}$), strong cap



Model equations

$$\frac{\partial C_i}{\partial t} = Mu C_1 - Md_i C_i + Md_{i+1} C_{i+1} \frac{\Delta z_{i+1}}{\Delta z_i} + \frac{1}{\Delta z_i} \left(\frac{K_{i+1/2} (C_{i+1} - C_i)}{\Delta z_{i+1/2}} + \frac{K_{i-1/2} (C_i - C_{i-1})}{\Delta z_{i-1/2}} \right)$$

where, $Md_i = Mu(h - z_{i-1/2}) / \Delta z_i$

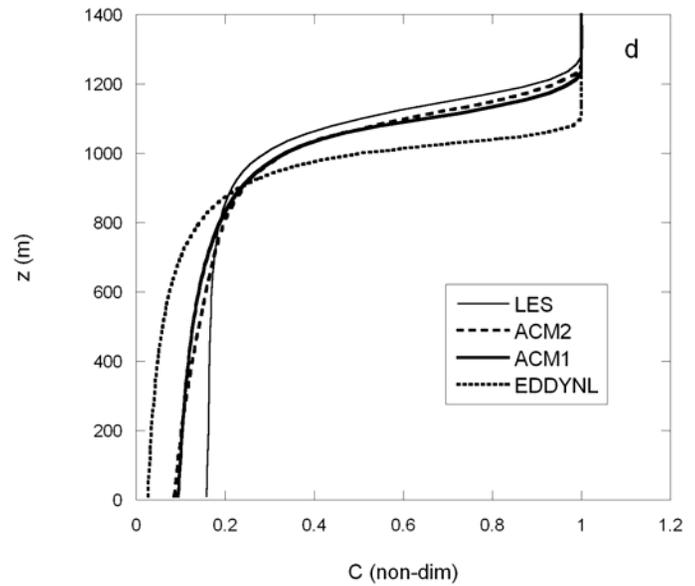
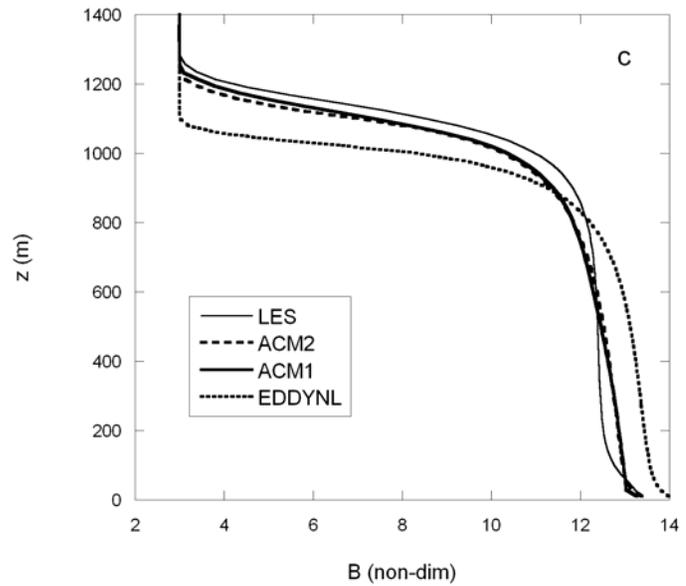
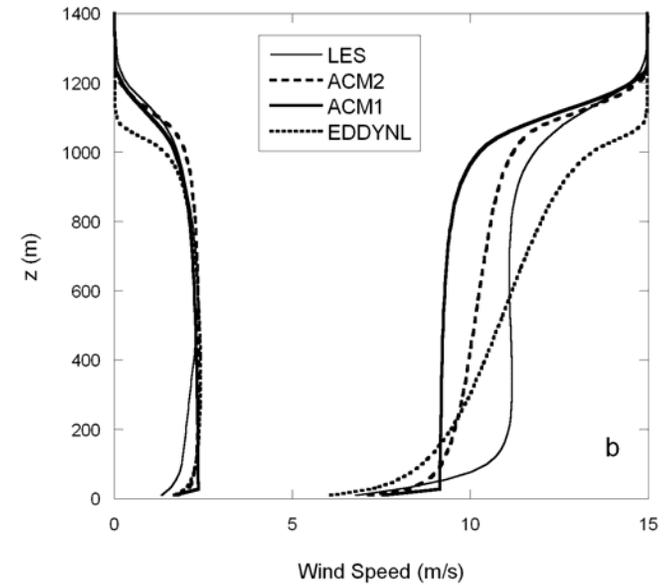
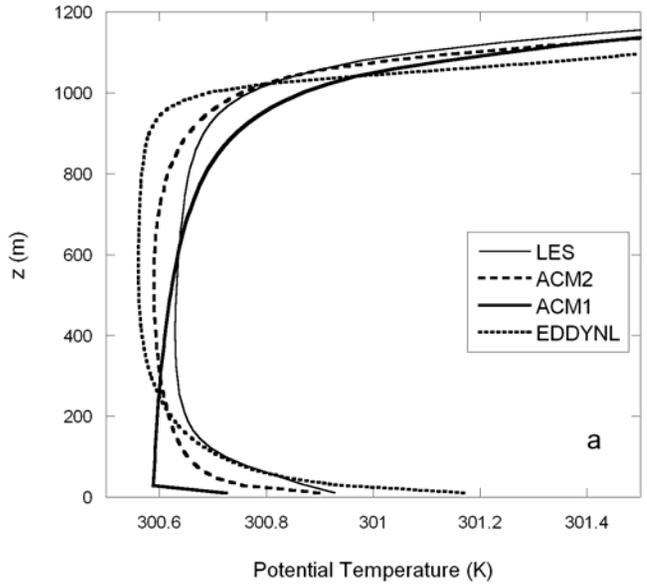
Mixing rates, all defined in terms of K_z and h , are partitioned into local and non-local components (f_{conv})

$$Mu = \frac{f_{conv} K_z(z_{1+1/2})}{\Delta z_1 (h - z_{1+1/2})}$$

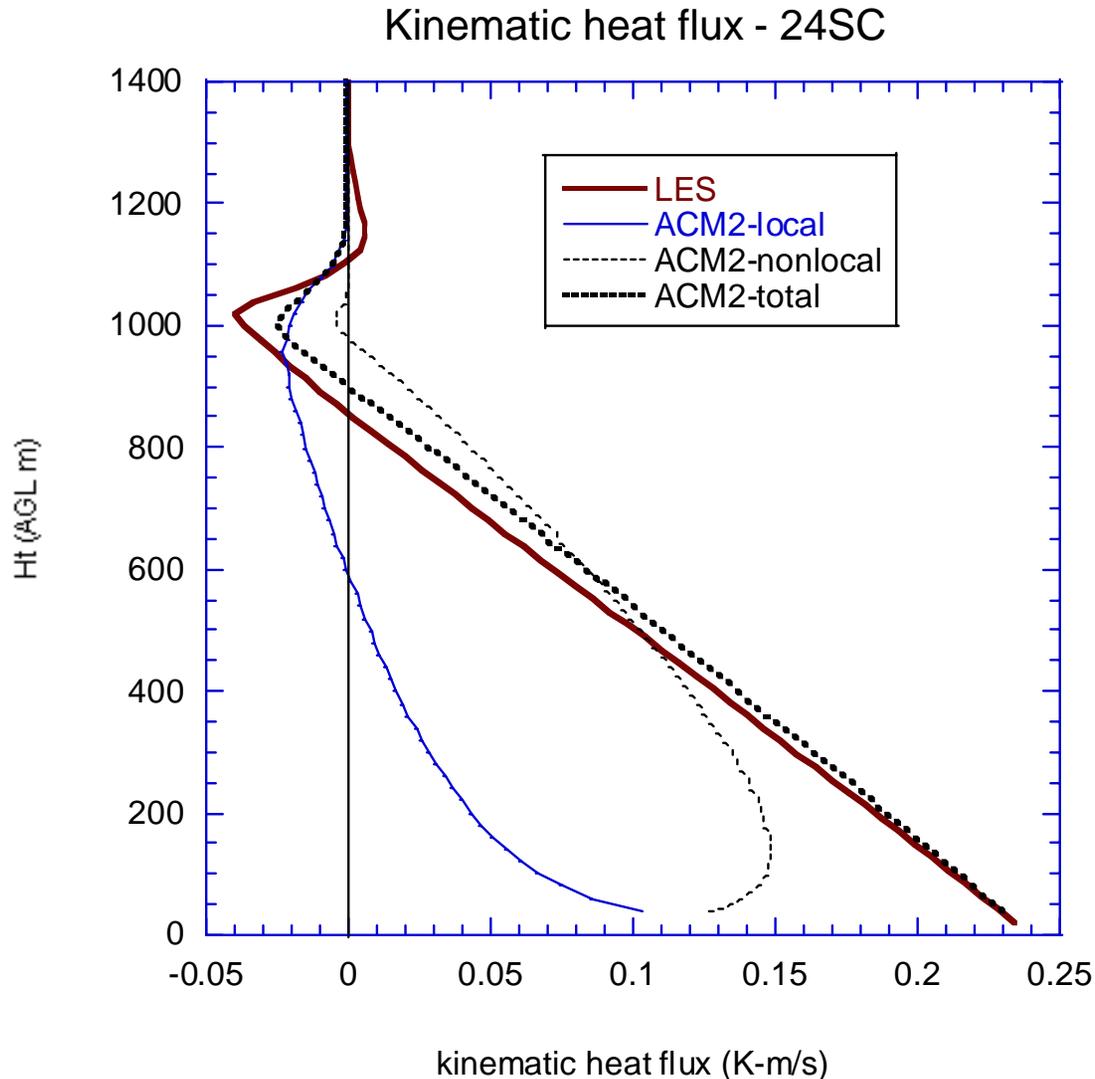
How to define f_{conv} ?

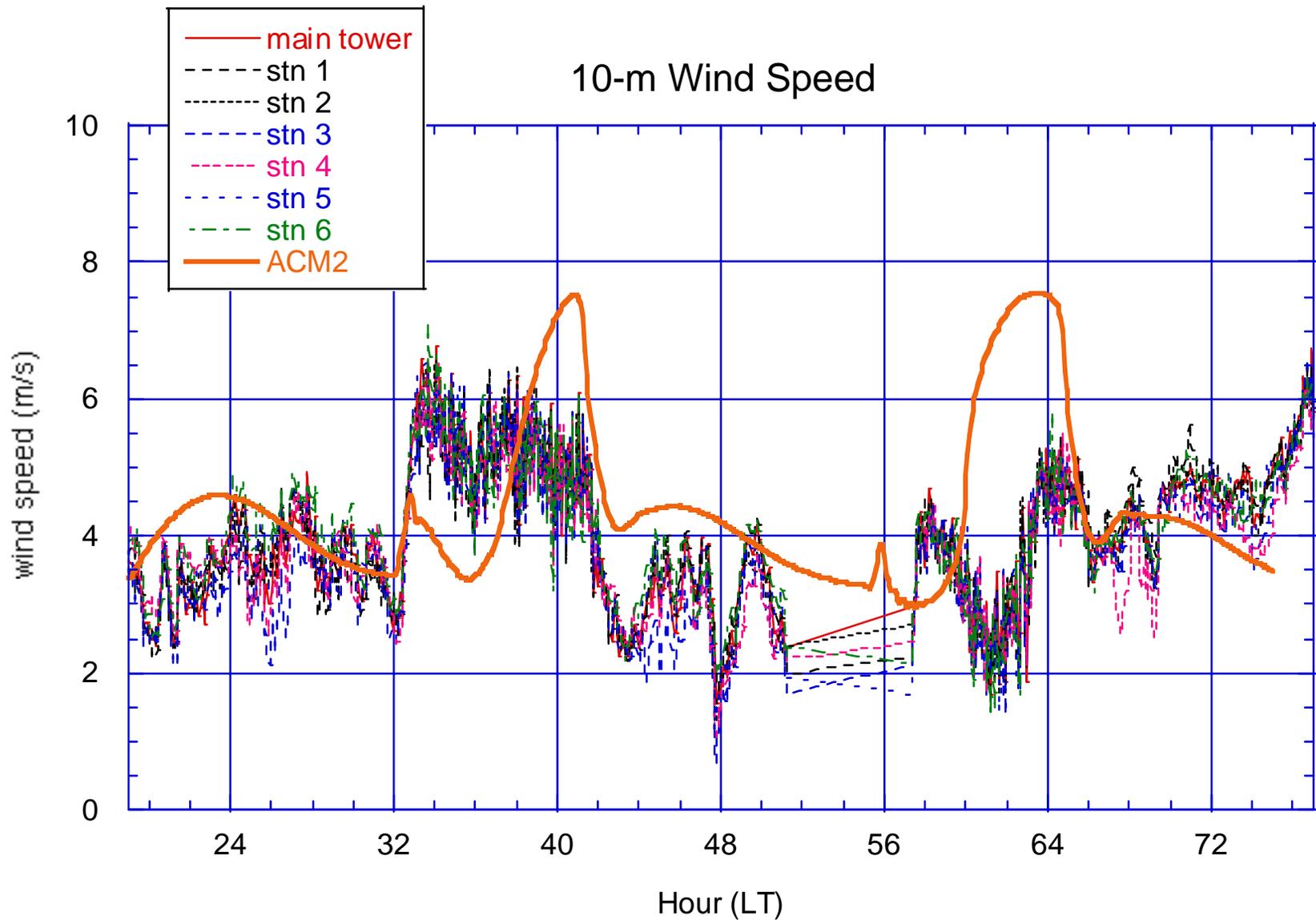
$$K_i = K_z(z)(1 - f_{conv})$$

Comparison of ACM2, ACM1 and EDDYNL (based on HB93) for 05WC case



Profiles of sensible heat flux. Local, non-local, and total sensible heat flux compared to LES





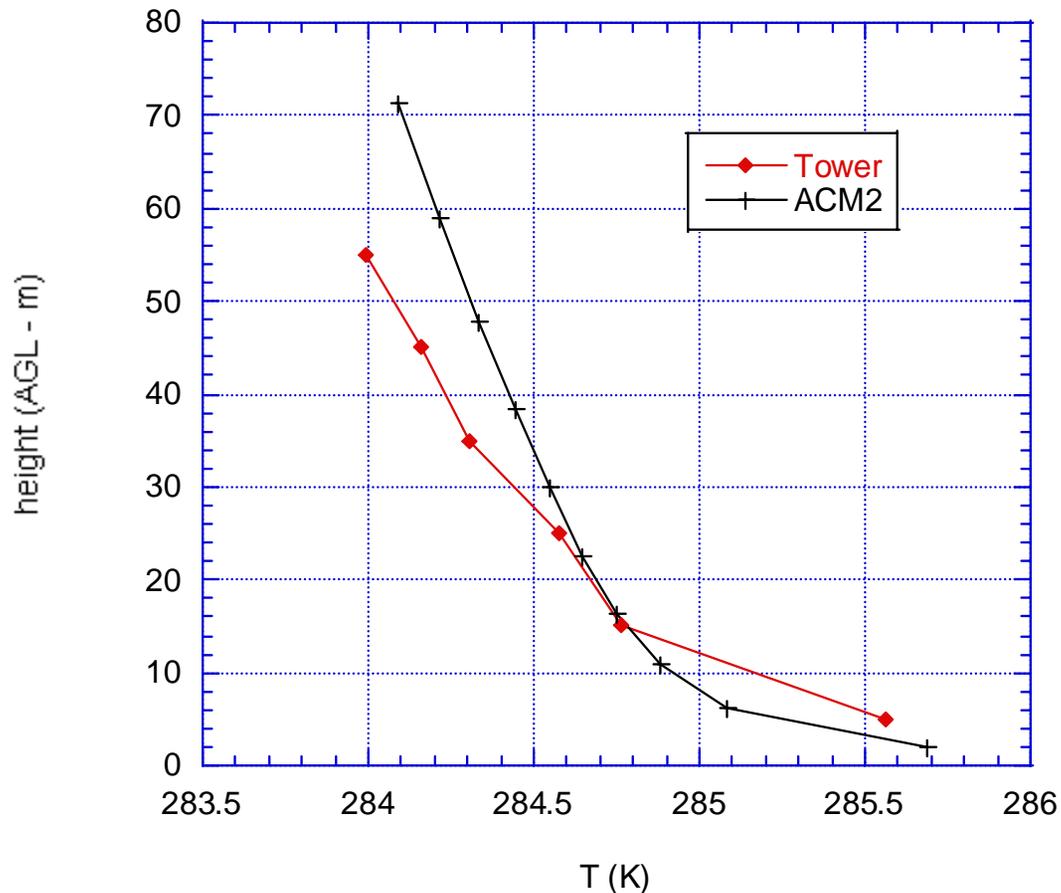
Model performance statistics for the 12 km MM5-ACM2 simulations over the period of July 13 – August 18, 2004

| | T | q_v | ws | wd |
|-------------|---------|------------|------------|----------|
| Data count | 398848 | 398848 | 398848 | 398848 |
| Correlation | 0.934 | 0.915 | 0.612 | --- |
| MAE | 1.42 K | 1.14 g/kg | 1.026 m/s | 31.8 deg |
| MB | 0.369 K | 0.109 g/kg | -0.211 m/s | 10.2 deg |
| Index of Ag | 0.931 | 0.911 | 0.606 | --- |



Near surface Temperature profile from CASES99 main tower

Temperature profile at 19Z (hr 38) October 23, 1999



Wind speed bias segregated by Landuse

